# Extending OpenSees for the Particle Finite Element Method

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#### Outline

- Motivation
- Particle Finite Element Method
  - Introduction to PFEM
  - Basic Equations
  - Fractional Step Method (FSM)
- 3 Implementation in OpenSees
  - Problems of the implementation of FSM
  - Options and solution to the implementation of FSM
  - Example
  - Mesh and Remesh
- Sensitivity Analysis of PFEM
  - Introduction to the sensitivity
  - Computing sensitivity
  - Example

#### Fluid-Structure Interaction

- Recent natural disasters
- Simulating structural response to wave loading



OSU's Hinsdale Wave Research Lab (www.flickr.com/photos/scottfrey)

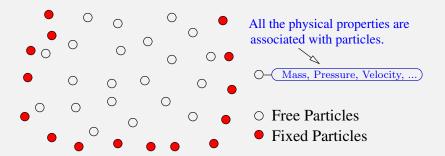
- Computational challenges
- The "OpenSees" homophone

- Lagrangian formulation
  - The position and physical properties of the particles are described in terms of the material or referential coordinates and time which is normally used in solid mechanics

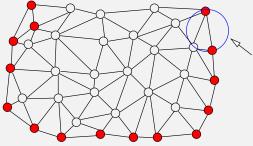
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  - Delaunay tessellation and Alpha shape method ⇒ mesh
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- Finite Element Method
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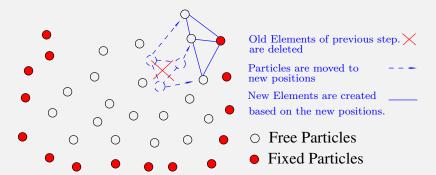


The Elements are created by using the Delaunay Tesselation.

The circumcircle of each element won't contain any other particles.

- Free Particles
- Fixed Particles

- Particle Based Method
- Finite Element Method
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Conservation Laws

Mass:

$$\frac{D\rho}{Dt} + \rho \frac{\partial u_i}{\partial x_i} = 0$$

Momentum:

$$\rho \frac{Du_i}{Dt} = -\frac{\partial}{\partial x_i} P + \frac{\partial}{\partial x_i} \sigma_{ij} + \rho f_i$$

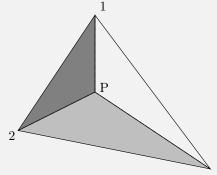
Where,

$$\rho$$
 – Density,  $u_i$  – Velocities  $x_i$  – Coordinates,  $P$  – Pressure  $\sigma_{ii}$  – Cauchy Stress,  $f_i$  – Body forces

• Linear interpolation (Unstable for incompressible continuum)

$$N_i = L_i$$
  $i = 1, 2, 3$  For 2D

Where,  $N_i$  is the shape function,  $L_i$  is the area coordinate for node i



For point P, the area coordinates

$$L_1 = \frac{areaP23}{area123}$$

$$L_2 = \frac{areaP13}{area123}$$

$$L_3 = \frac{areaP12}{area123}$$

Discretized equations (stabilized by Finite Calculus Method)

$$\mathbf{M}\dot{\mathbf{U}} + \mathbf{K}\mathbf{U} = \mathbf{F}$$

where.

$$\mathbf{M} = \begin{bmatrix} \bar{\mathbf{M}} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} \end{bmatrix}$$
$$\mathbf{K} = \begin{bmatrix} \bar{\mathbf{K}} & -\mathbf{G} & \mathbf{0} \\ \mathbf{G}^T & \mathbf{L} & \mathbf{Q} \\ \mathbf{0} & \mathbf{Q}^T & \hat{\mathbf{M}} \end{bmatrix}$$
$$\mathbf{F} = \begin{bmatrix} \bar{\mathbf{F}} & \mathbf{0} & \mathbf{0} \end{bmatrix}^T$$

$$\begin{aligned} \mathbf{U} &= \begin{bmatrix} \mathbf{v} & \mathbf{p} \end{bmatrix}^T \\ \dot{\mathbf{U}} &= \begin{bmatrix} \dot{\mathbf{v}} & \dot{\mathbf{p}} \end{bmatrix}^T \end{aligned}$$

M - Mass matrix

K - Stiffness matrix

**G** – Gradient operator

L – Laplacian operator

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Blue matrices are related to the stability issues of incompressible fluid.

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To overcome this problem, the fractional step method (FSM) is used to solve the discretized equations.

Predictor of velocity v\*

$$\mathbf{v}^* = \mathbf{v}^n - \Delta t \mathbf{ar{M}}^{-1} \left[ \mathbf{ar{K}} \mathbf{v}^j - \mathbf{G} \mathbf{p}^j - \mathbf{f} 
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$$\delta \mathbf{p} = -(\mathbf{L} + \Delta t \mathbf{S})^{-1} \left[ \mathbf{G}^{\mathsf{T}} \mathbf{v}^* + \mathbf{Q} \mathbf{\pi}^j + \mathbf{L} \mathbf{p}^j 
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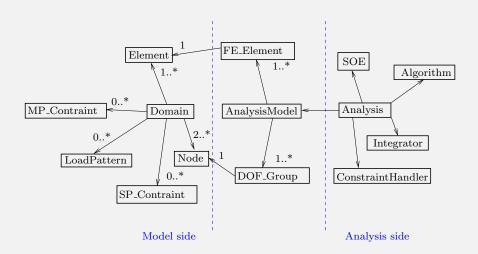
• Pressure gradient  $\pi^{j+1}$ 

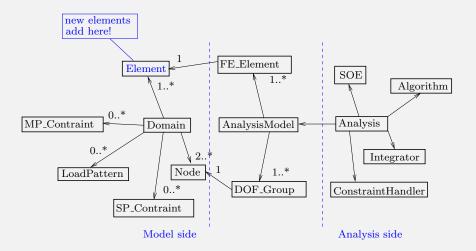
$$oldsymbol{\pi}^{j+1} = -\hat{\mathbf{M}}^{-1} \mathbf{Q}^T \mathbf{p}^{j+1}$$

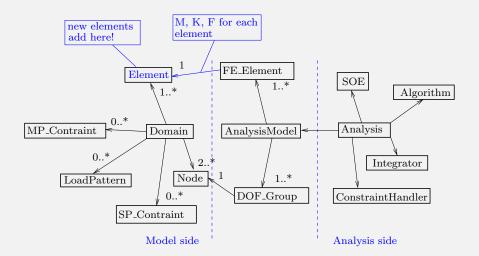
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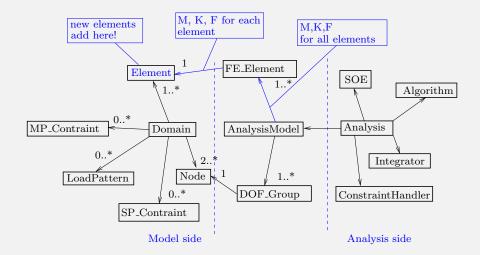
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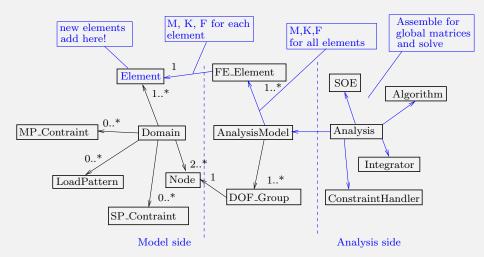
## OpenSees class diagram











• FSM requires partitioned matrices since velocity and pressure are separated,

$$\mathbf{M} = \begin{bmatrix} \bar{\mathbf{M}} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} \end{bmatrix}, \quad \mathbf{K} = \begin{bmatrix} \bar{\mathbf{K}} & -\mathbf{G} & \mathbf{0} \\ \mathbf{G}^{\mathcal{T}} & \mathbf{L} & \mathbf{Q} \\ \mathbf{0} & \mathbf{Q}^{\mathcal{T}} & \hat{\mathbf{M}} \end{bmatrix}, \quad \mathbf{F} = \begin{bmatrix} \bar{\mathbf{F}} \\ \mathbf{0} \\ \mathbf{0} \end{bmatrix}$$

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• Matrices multiplications and inversions are applied on the partitioned matrices. Therefore partitioning of matrices has to be performed at the global level. Three inversions,  $\bar{\mathbf{M}}^{-1}$ .  $\mathbf{S}^{-1}$ and  $\hat{\mathbf{M}}^{-1}$  occur in a single iteration while normally there is only one in OpenSees.

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- From the flow chart shown before, global matrices are only available in the analysis side. So we can only partition matrices in the analysis side.

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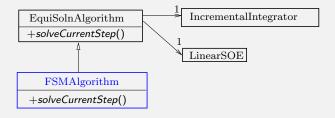
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- Model side? Analysis side?

#### Option 1: add a new algorithm

The first option is to implement FSM in a new algorithm FSMAlgorithm,

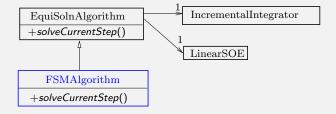
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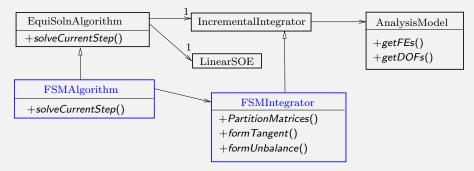
We want use FSMAlgorithm to partition matrices in the global level. But FSMAlgorithm does not have the DOFs information. To get the information, another new class PFEMIntegrator has to be added also.

# Option 2: add a new algorithm and integrator

The second option is to create both an algorithm and integrator,

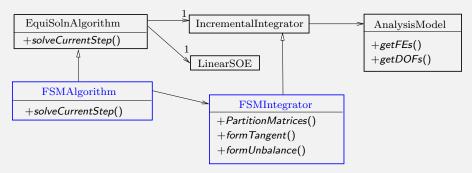
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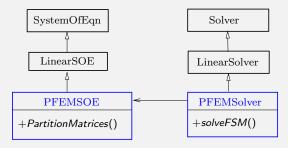
However, this implementation makes the algorithm and integrator too specialized for FSM and needs new methods in the interface of the FSM algorithm and integrator. The FSM algorithm and integrator are coupled to the model information.

#### Option 3: Add a SOE and solver

The third option is to add a LinearSOE and Solver,

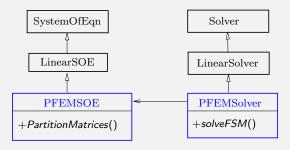
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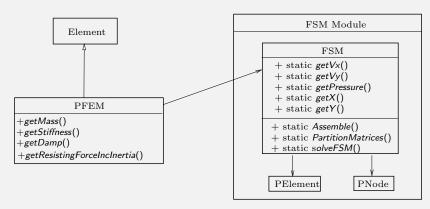
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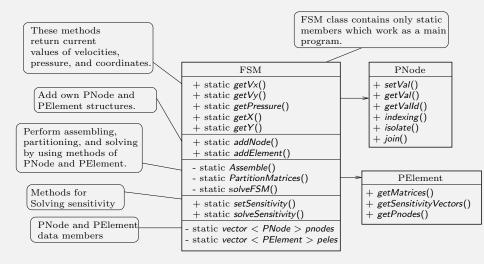


This option has the same problem with option 1 that neither LinearSOE nor Solver knows the DOFs information. They cannot partition without knowing IDs and only work with each other.

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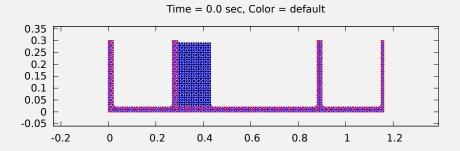
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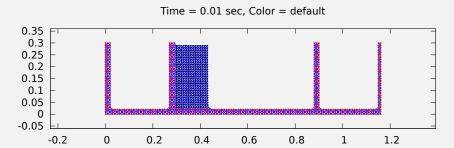
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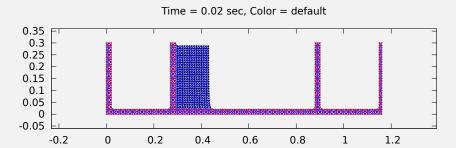
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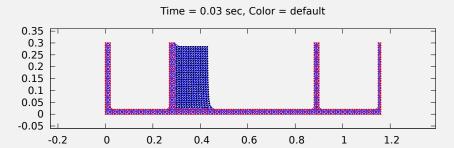
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- PNode and PElement are standalone structures used by FSM for storing its nodes and elements

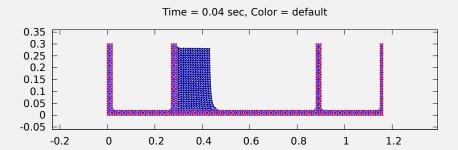
- A standard test problem of PFEM, involving large domain changing and strong nonlinearity.
- A water column is kept in a container by an unseen vertical board. Start by removing the board.

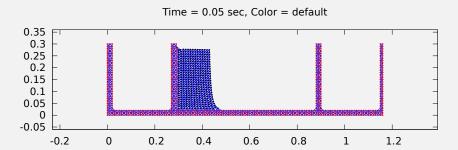


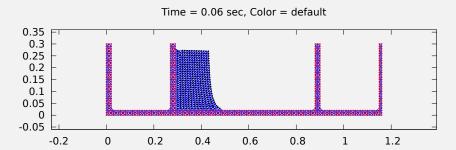


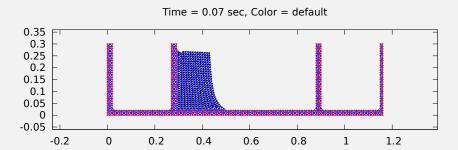


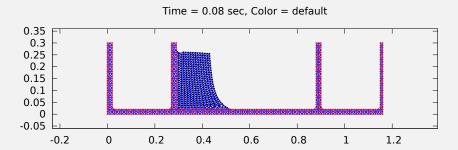


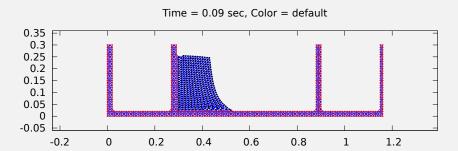


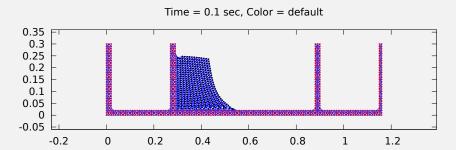


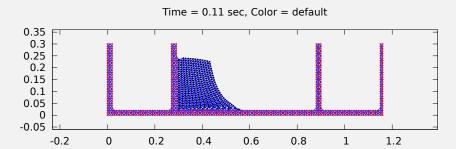


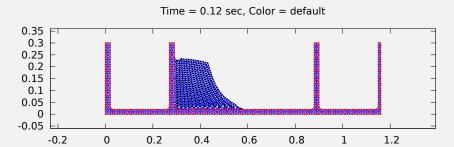


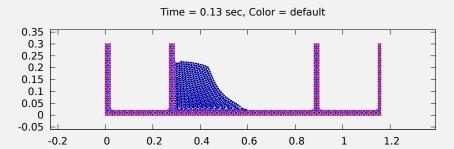


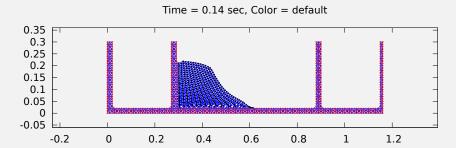


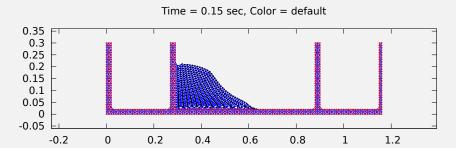


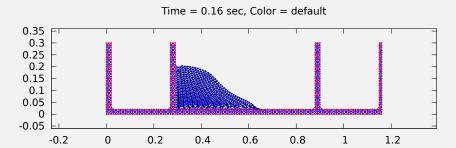


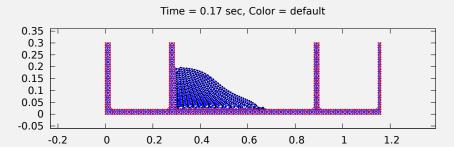


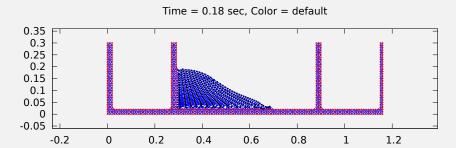


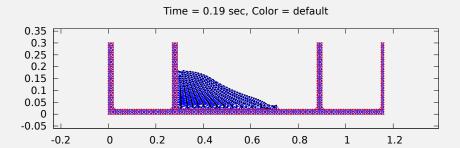


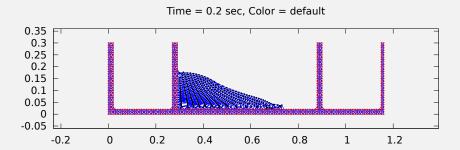


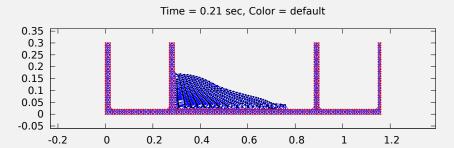


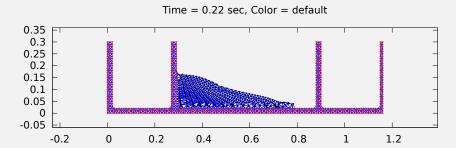


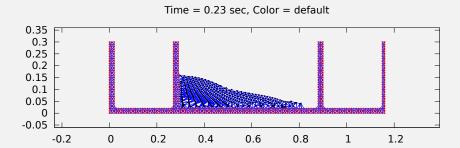


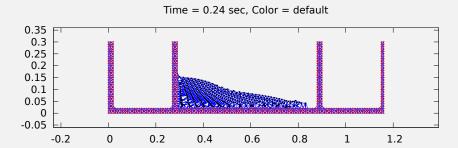


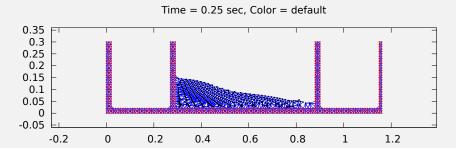


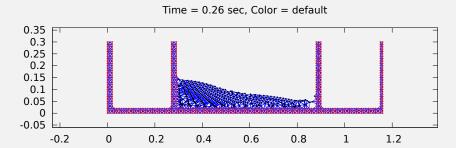


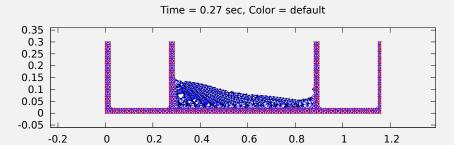


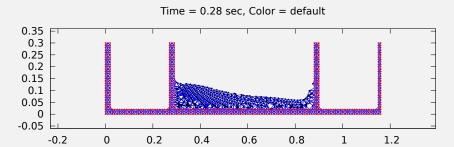


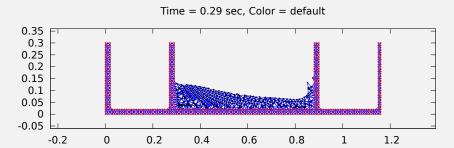


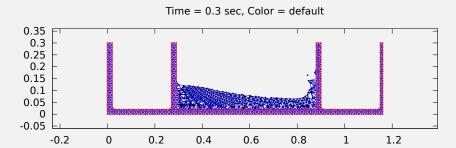


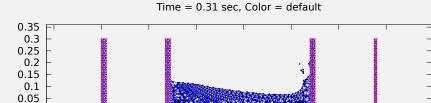












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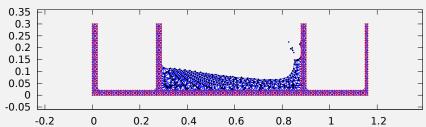
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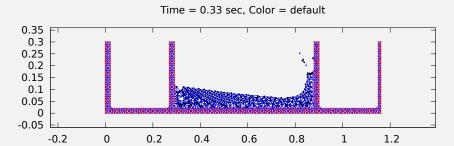
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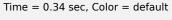
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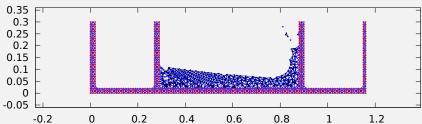
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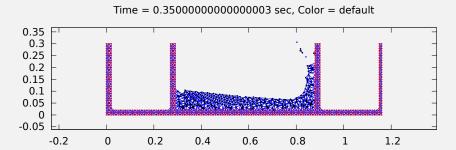




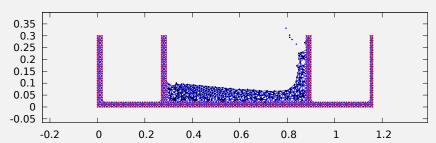




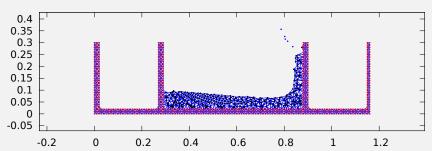


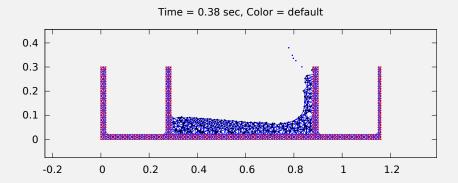


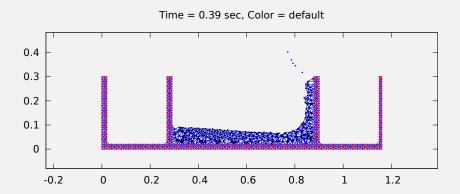


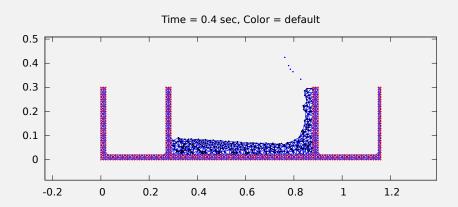


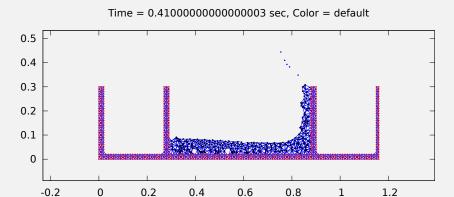


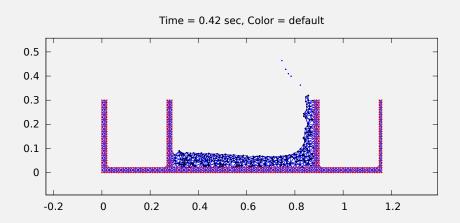


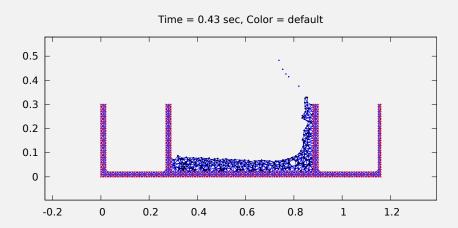


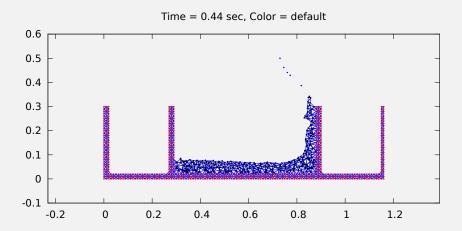


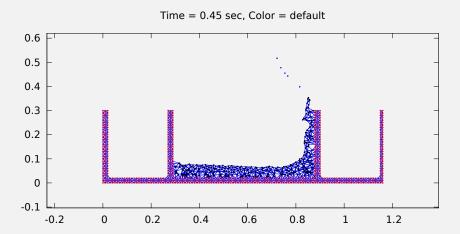


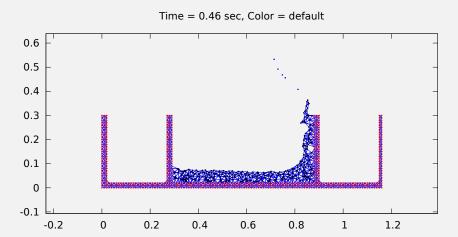


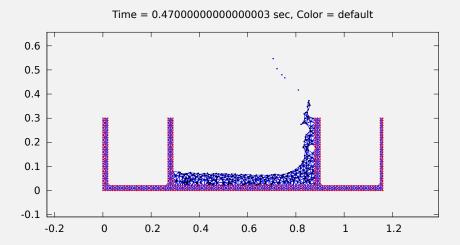


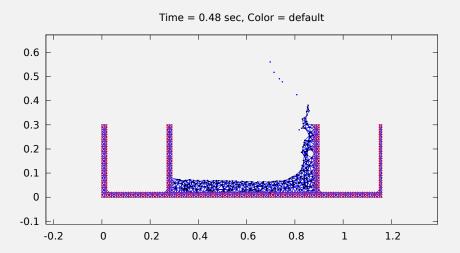


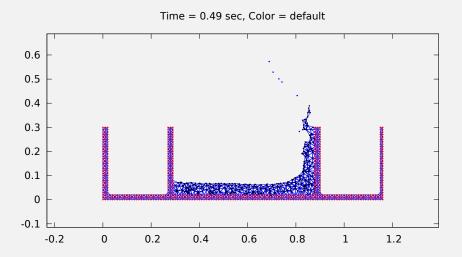


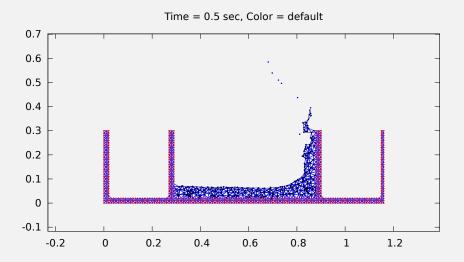


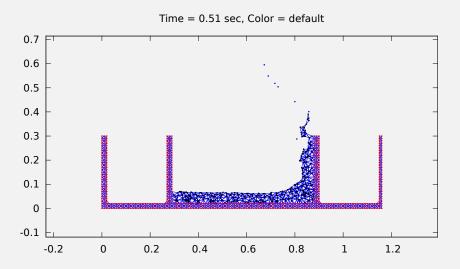


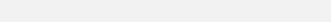


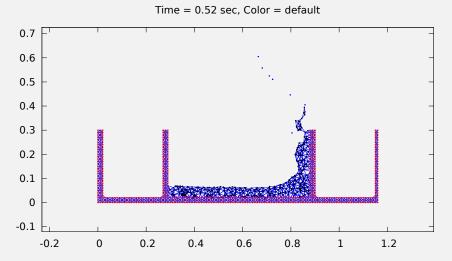


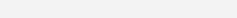


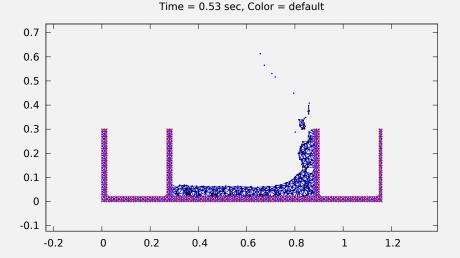




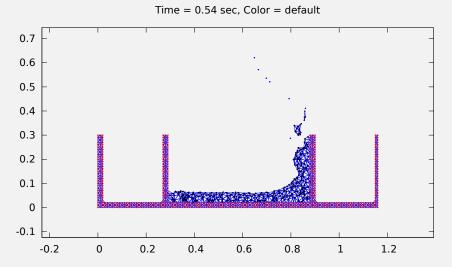


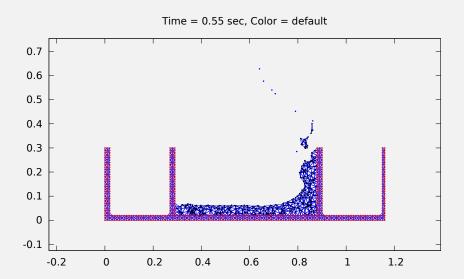


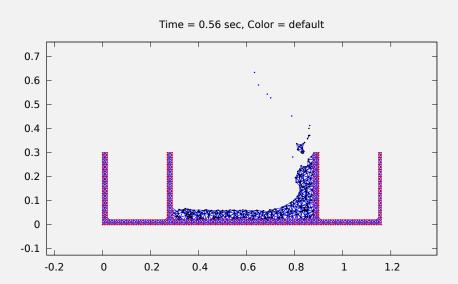




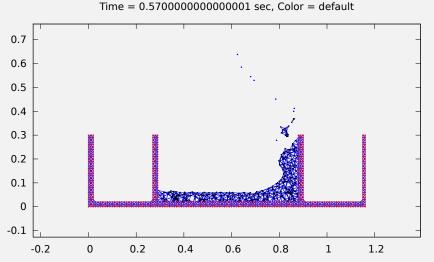


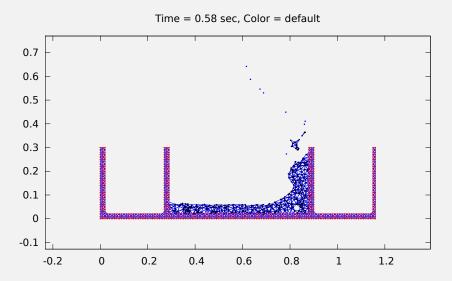


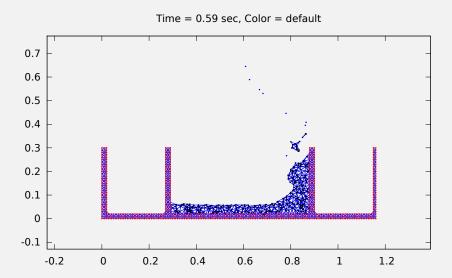


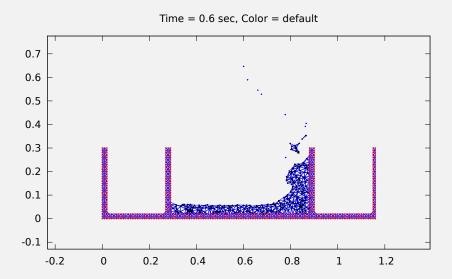


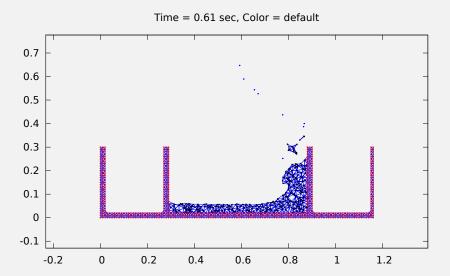


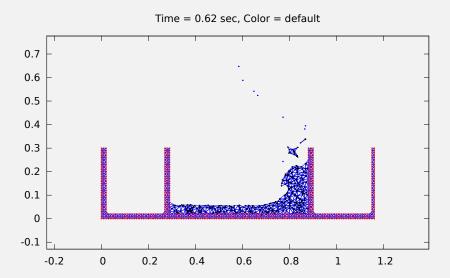


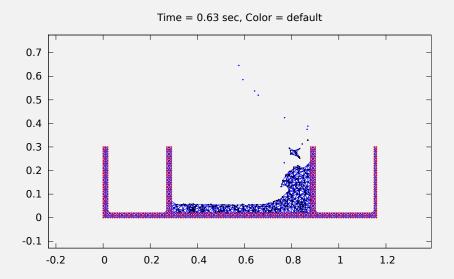


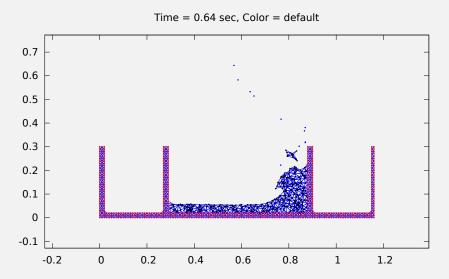


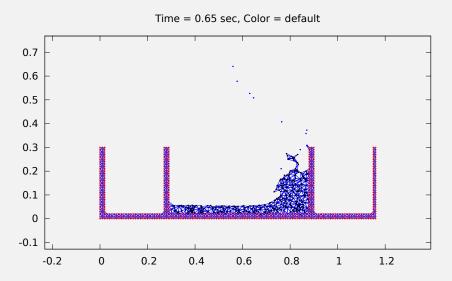


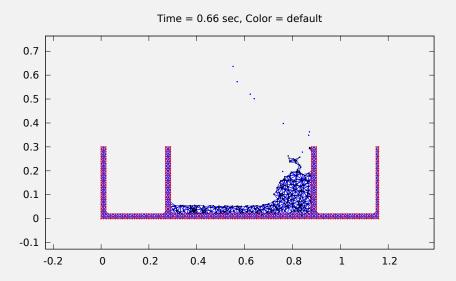


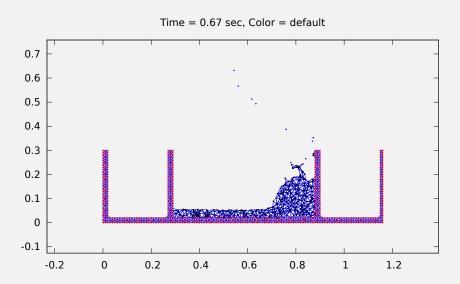


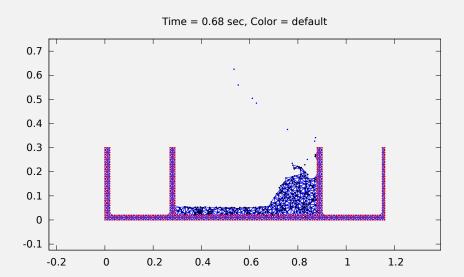


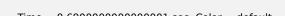


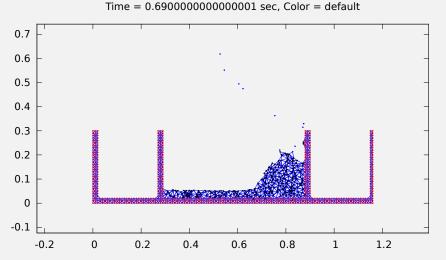


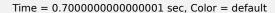


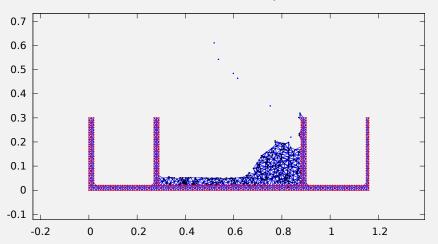


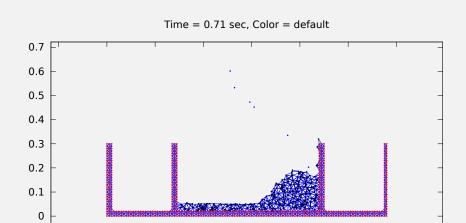












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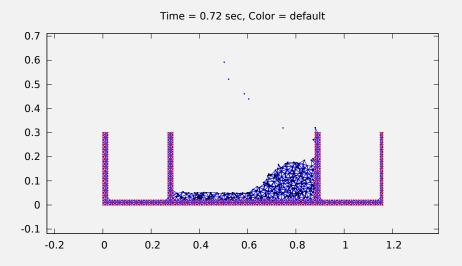
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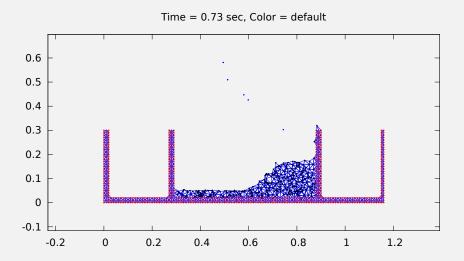
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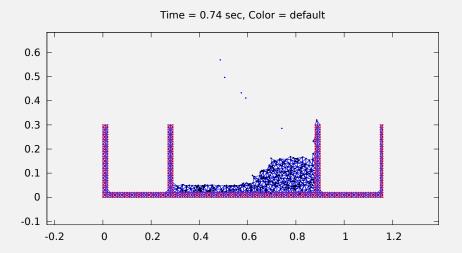
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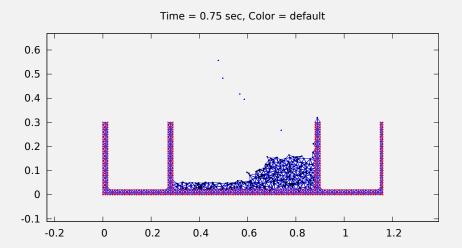
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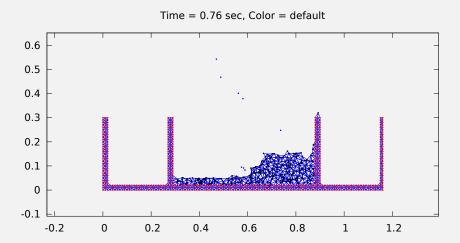
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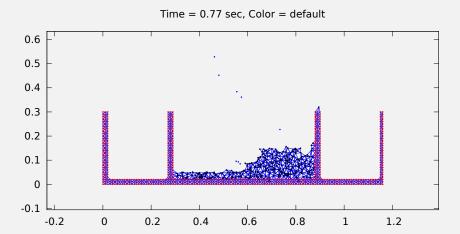


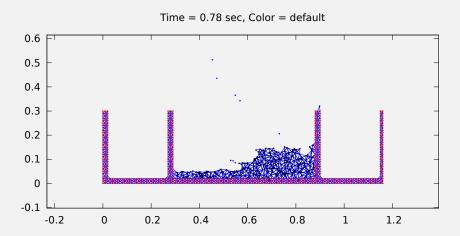


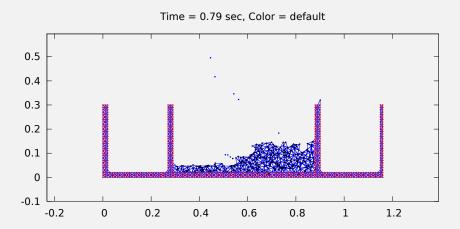


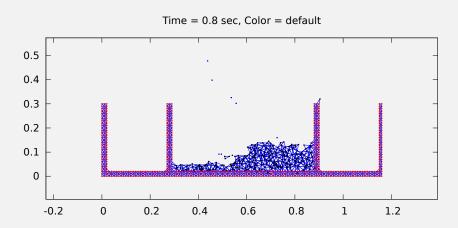


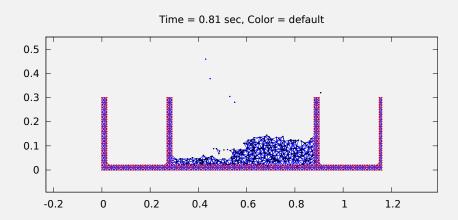


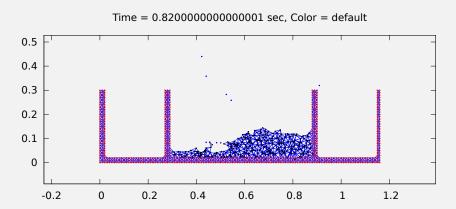


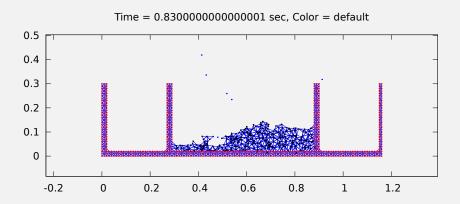


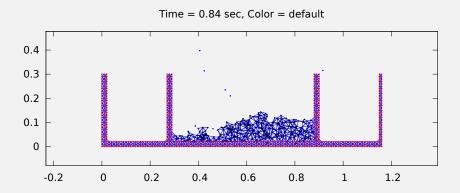


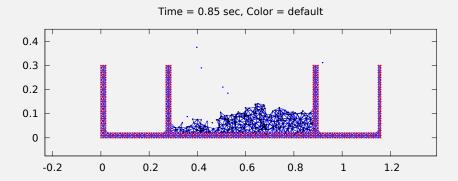


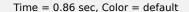


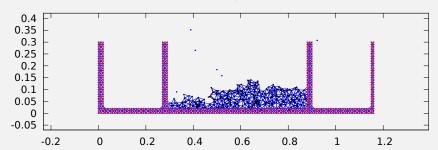


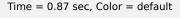


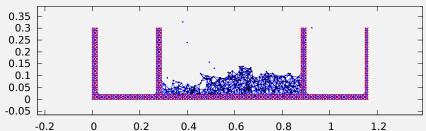


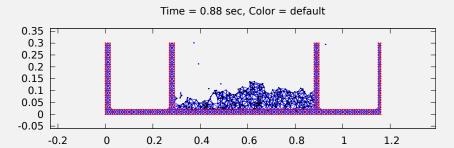


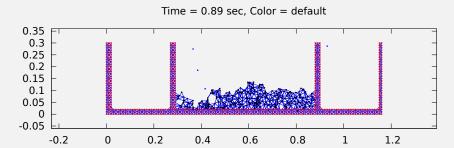


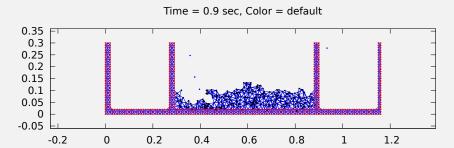


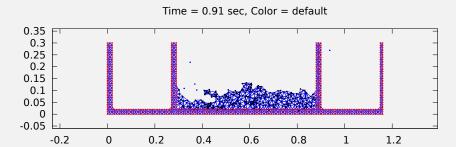


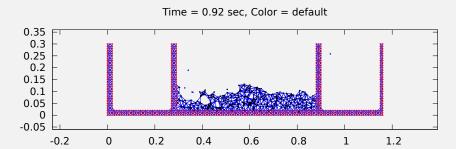


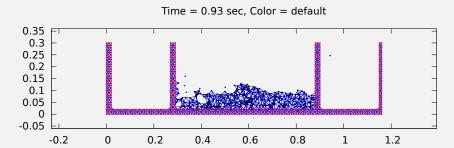


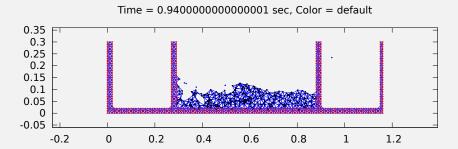


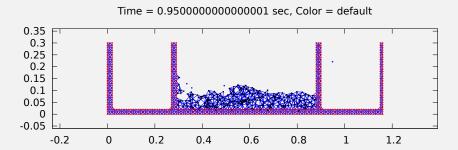


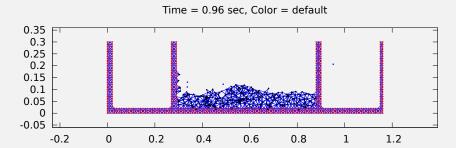


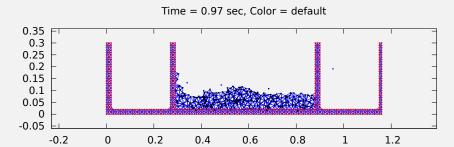


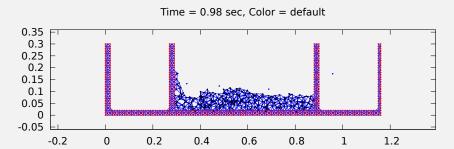


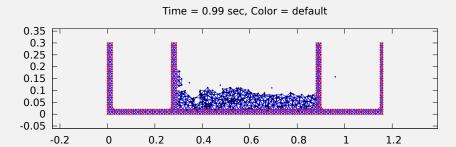


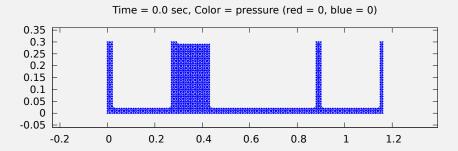


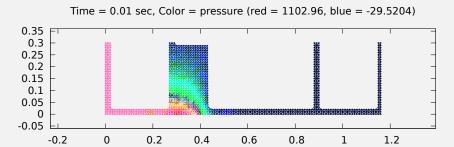


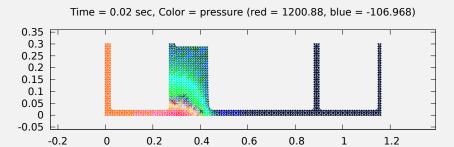


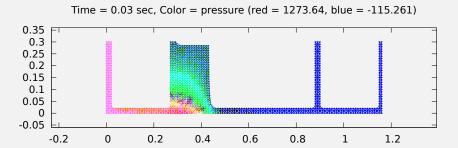


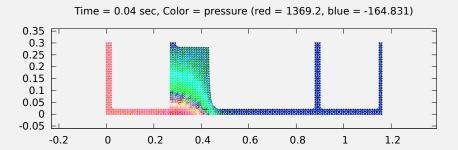


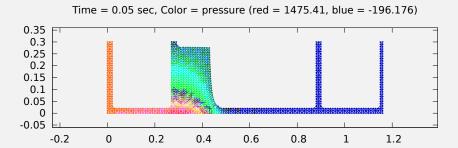


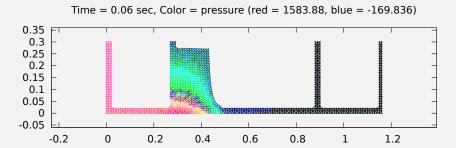


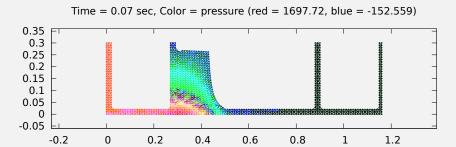


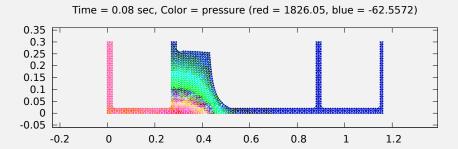


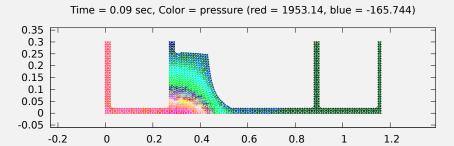


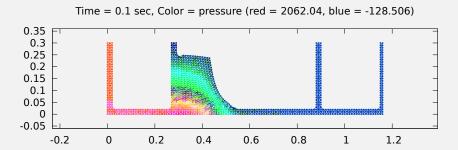


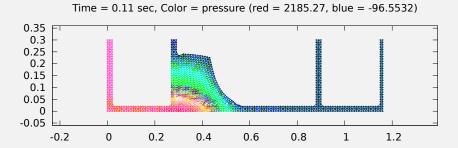


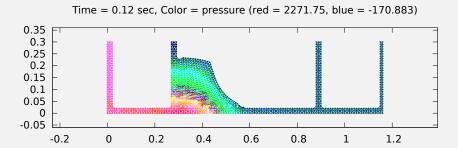


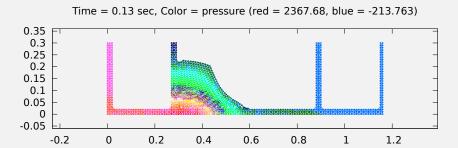


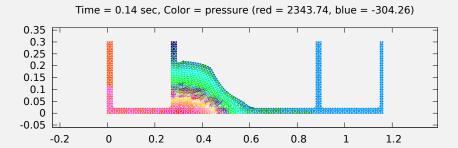


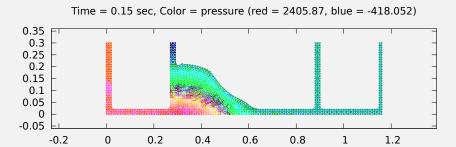


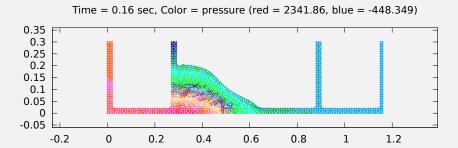


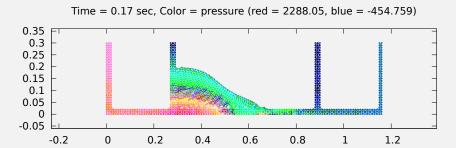


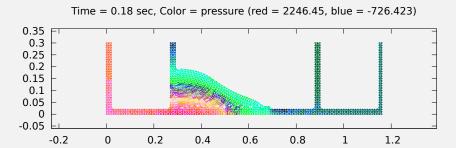


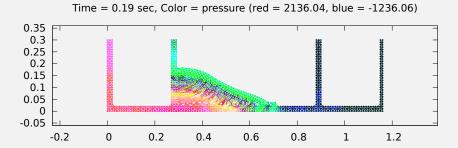


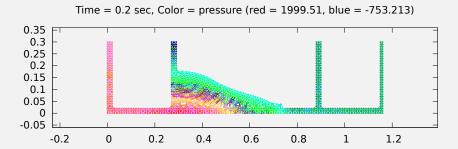


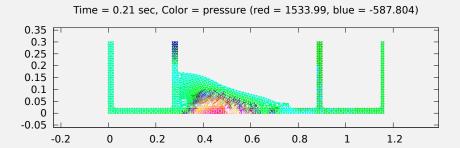


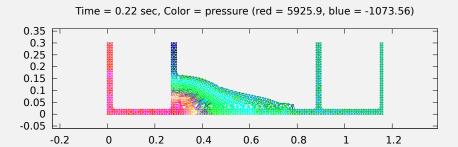


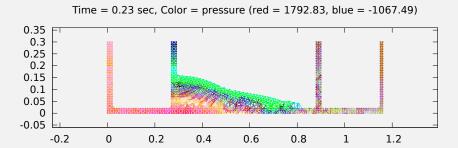


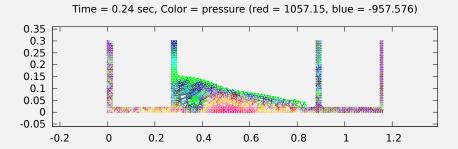


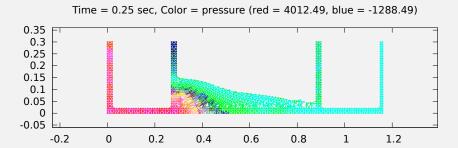


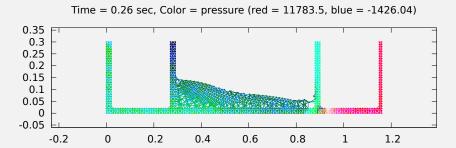


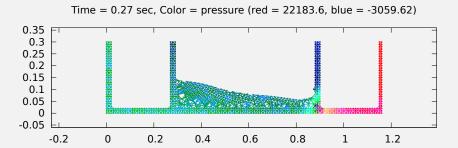


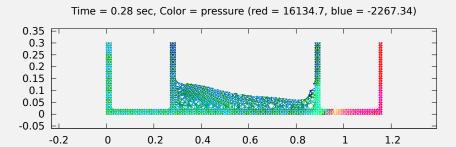


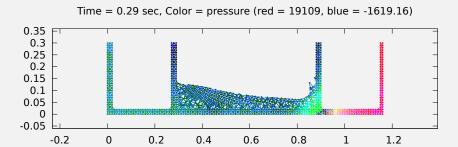


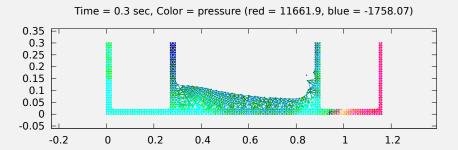


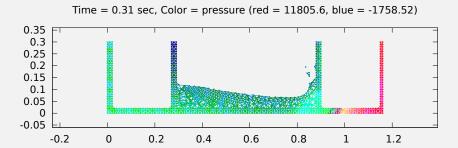


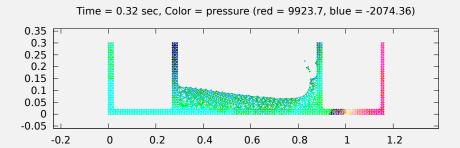


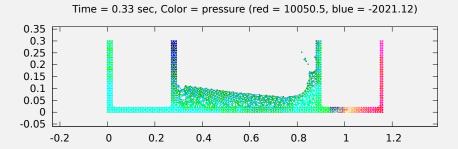


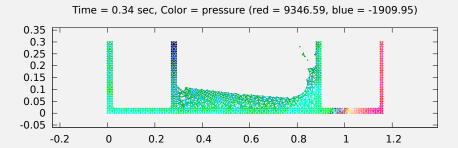




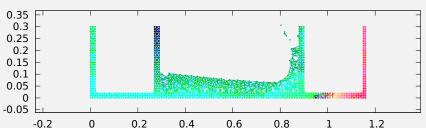


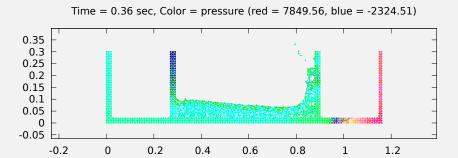


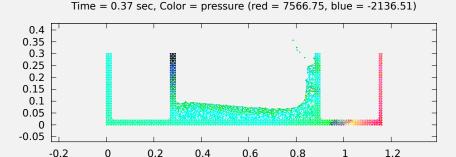


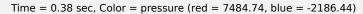


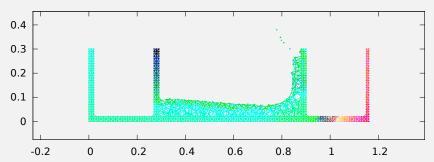
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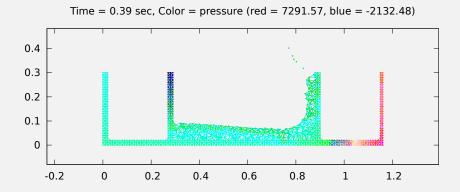


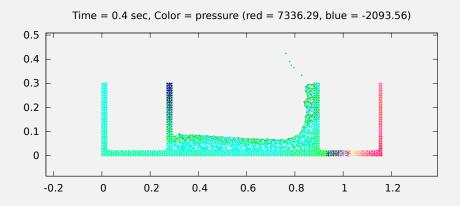




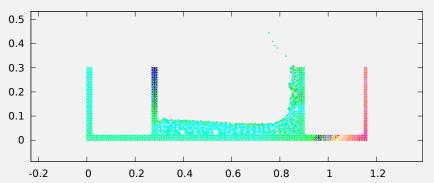


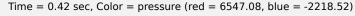


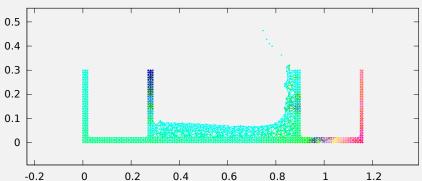


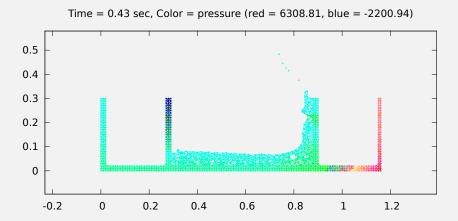


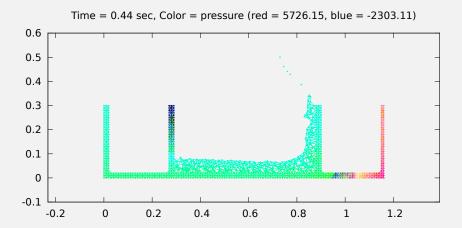
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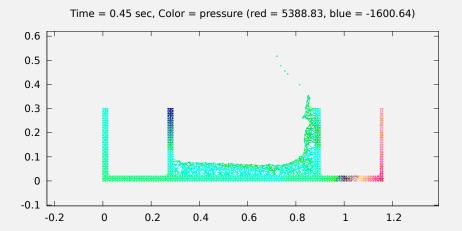


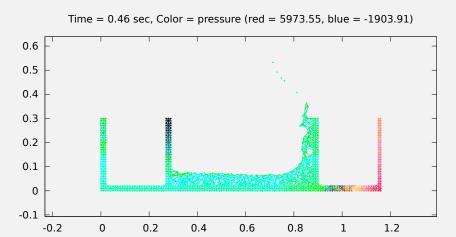




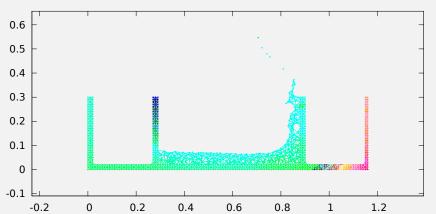


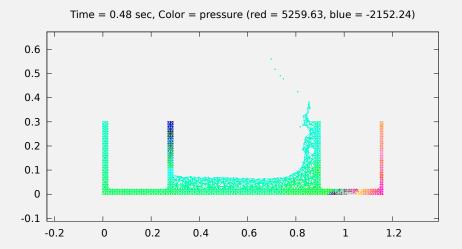


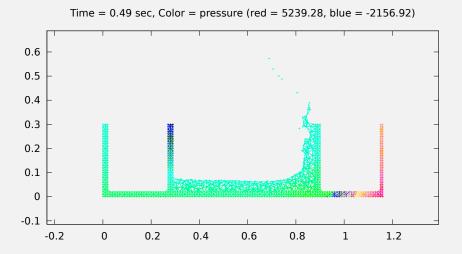


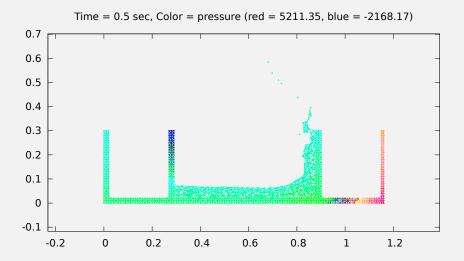


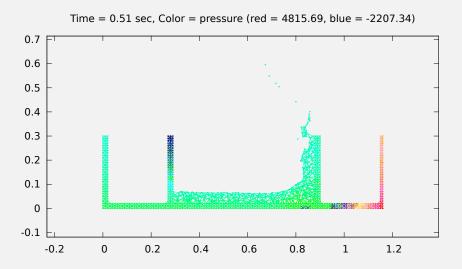
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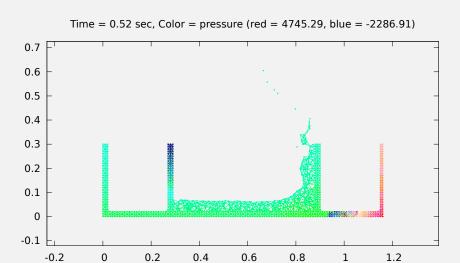


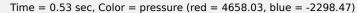


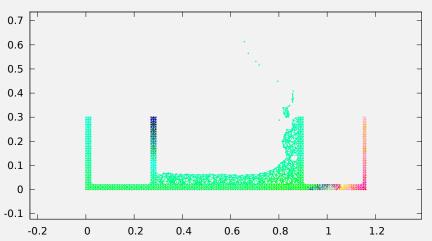


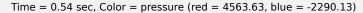


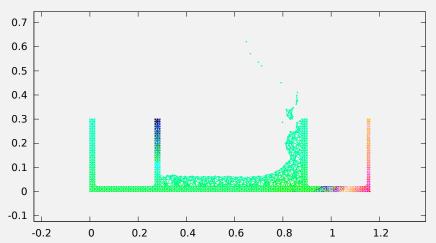




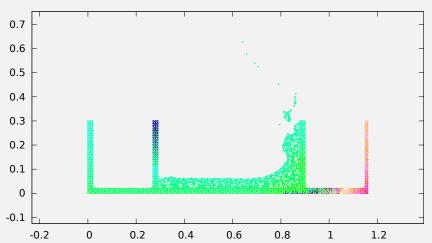




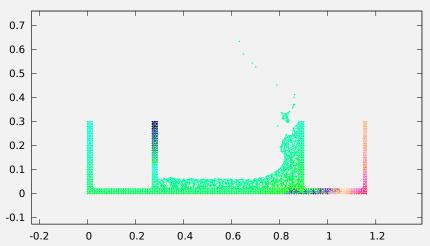




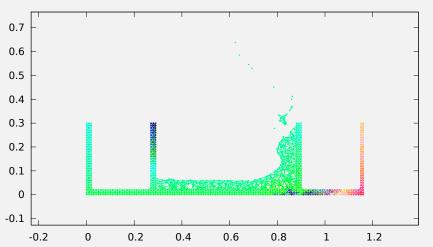
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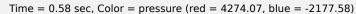


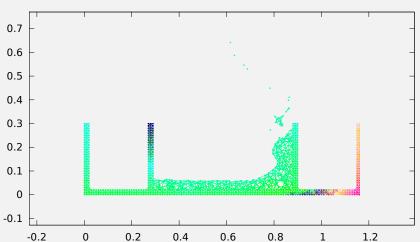


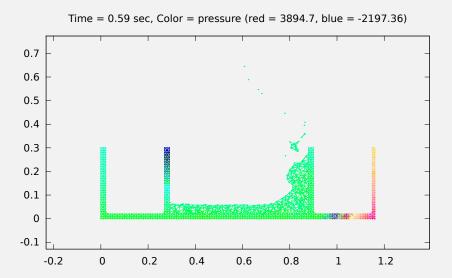


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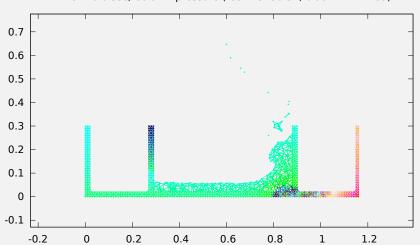


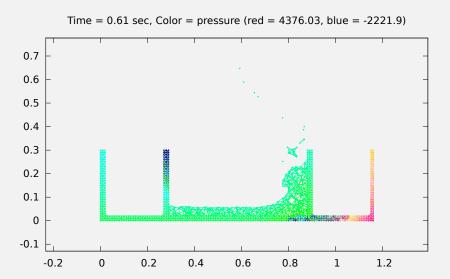


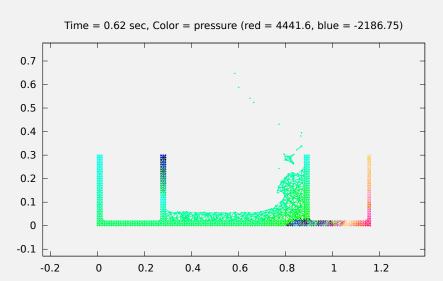


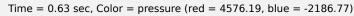


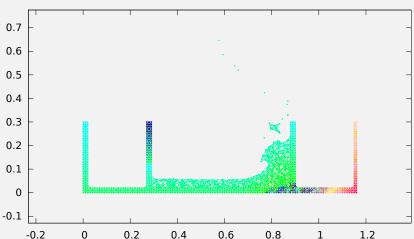
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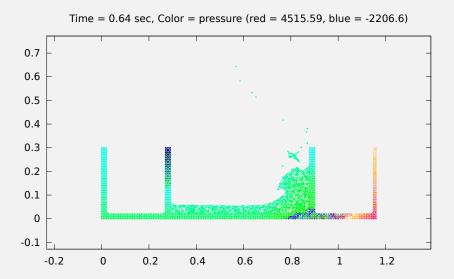


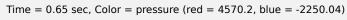


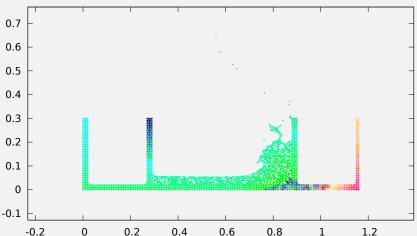




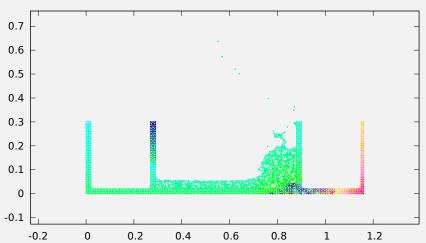


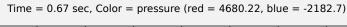


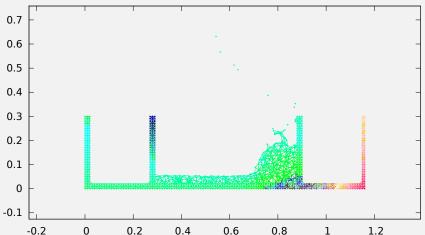


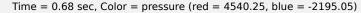


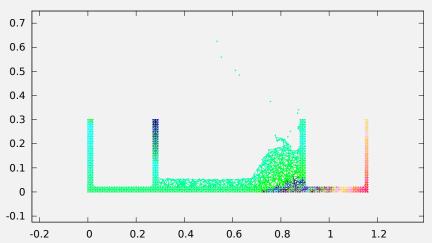


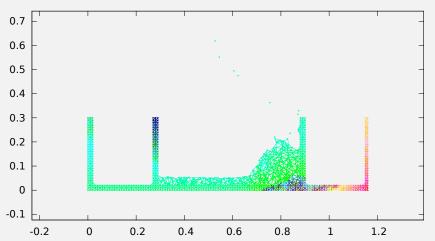




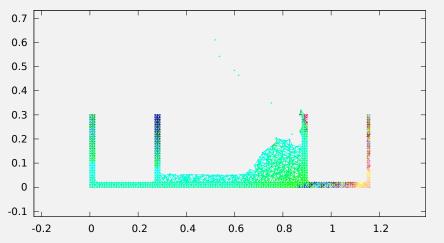


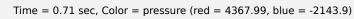


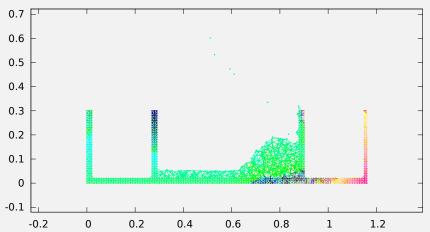


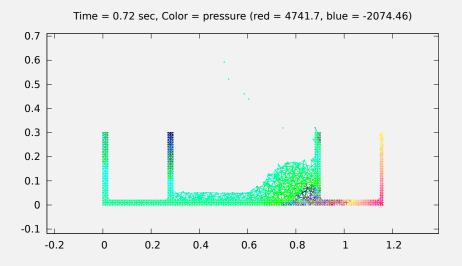


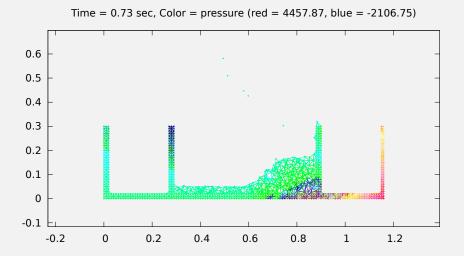
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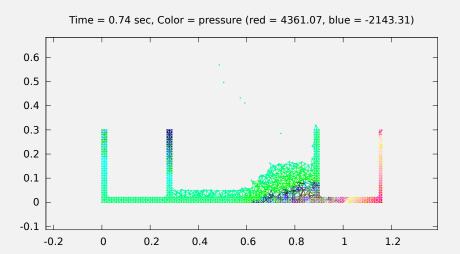


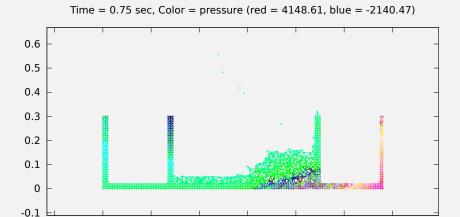












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0.2

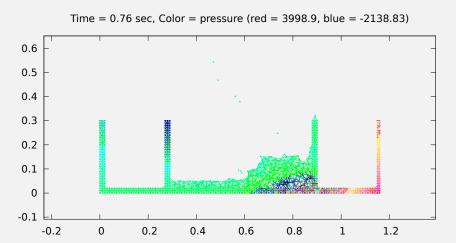
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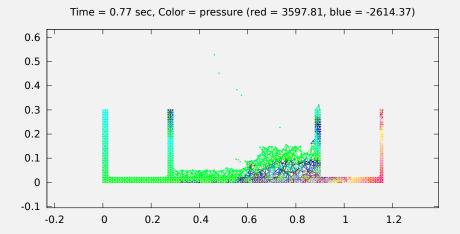
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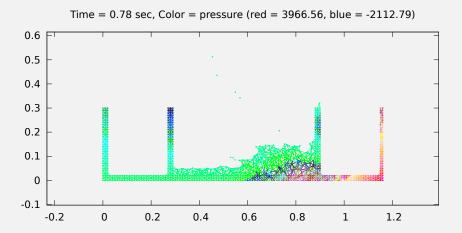
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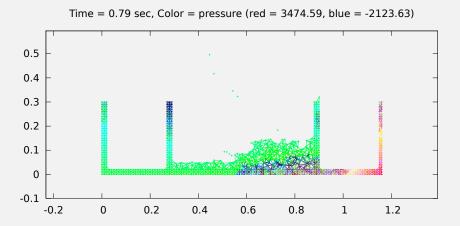
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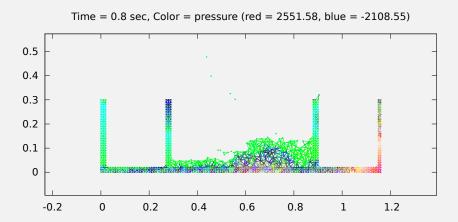
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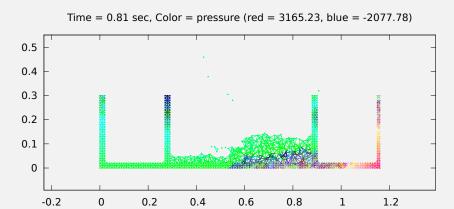


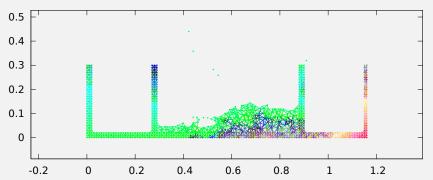


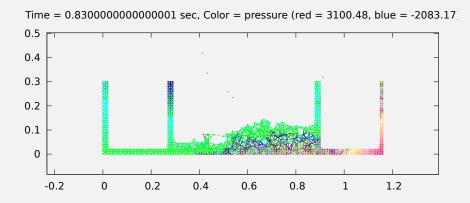


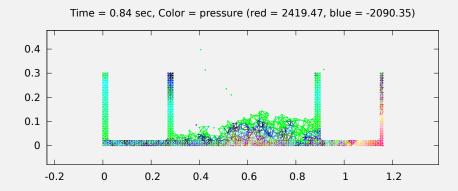


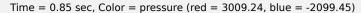


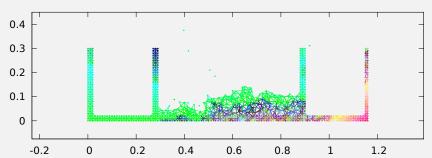


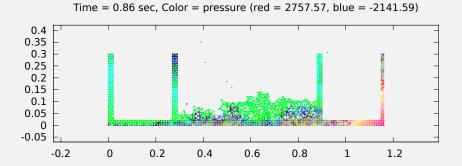


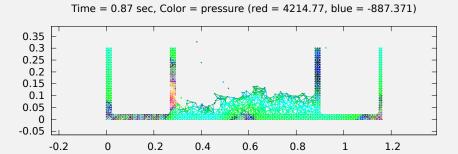


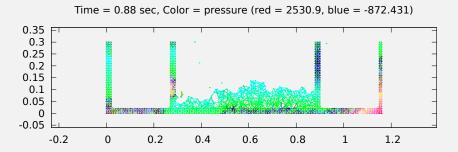


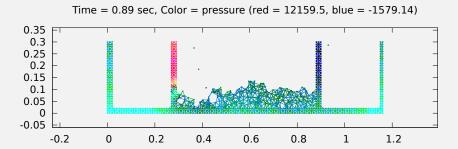


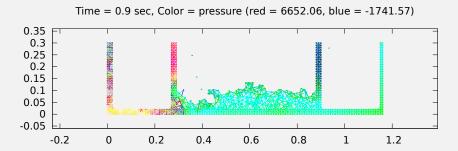


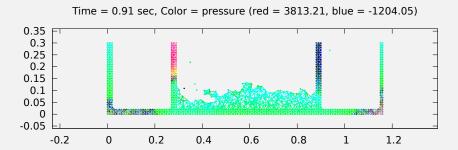


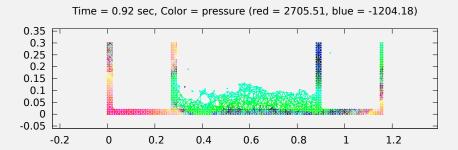


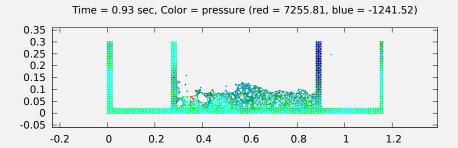


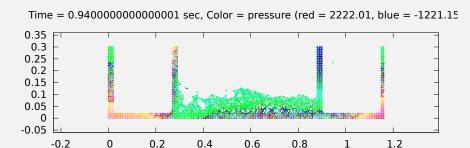


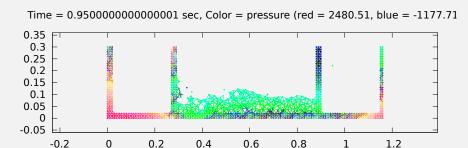


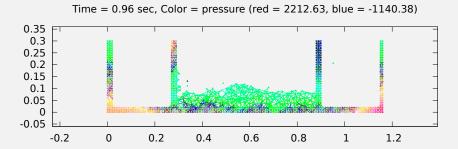


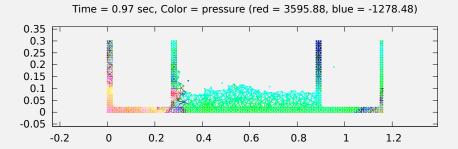


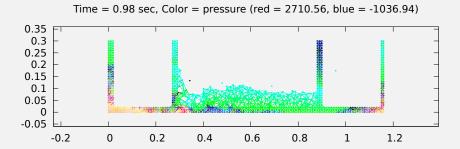


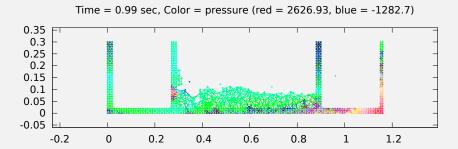












#### Mesh and Remesh

The mesh and remesh are based only on nodal positions and done by using the Delaunay Triangulation and Alpha Shape.

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- Alpha Shape is a generalization of the convex hull of a set of nodes. Let  $\alpha$  a real number with  $0 < \alpha < \infty$ . For  $\alpha = \infty$ , the Alpha Shape is identical to the Delaunay Triangulation. For  $\alpha = 0$ , the Alpha Shape shrinks to the set of nodes. Setting  $\alpha$ to a appropriate value can remove the unnecessary triangles to recover the real boundaries.

A Tcl script delaunayTri.tcl is used to mesh the domain,

• In each time step, the current coordinates of all nodes are passed to procedure delaunayTri

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- External program qhull is executed in Tcl to do the Delaunay Triangulation based on the nodal positions

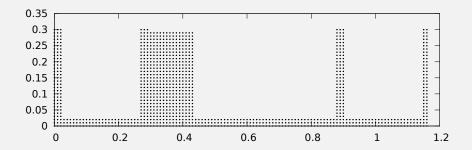
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- External program qhull is executed in Tcl to do the Delaunay Triangulation based on the nodal positions
- The area, radius, size of each triangle in the triangulation are calculated
- Alpha shape test is performed on each triangle. For triangles failed on the test are removed from the triangulation
- Remaining triangles are elements to be created in OpenSees.

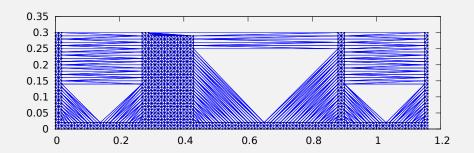
## Example of meshing

At each time step, a set of nodes are given



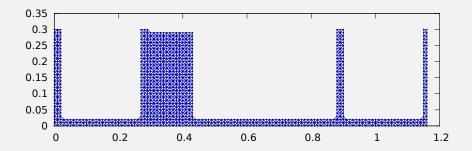
## Example of meshing

Delaunay Triangulation of the set of nodes is calculated



## Example of meshing

Alpha Shape of the set of nodes (lpha= 1.4) is calculated



#### Outline

- Motivation
- Particle Finite Element Method
  - Introduction to PFEM
  - Basic Equations
  - Fractional Step Method (FSM)
- 3 Implementation in OpenSees
  - Problems of the implementation of FSM
  - Options and solution to the implementation of FSM
  - Example
  - Mesh and Remesh
- Sensitivity Analysis of PFEM
  - Introduction to the sensitivity
  - Computing sensitivity
  - Example

#### **Definition**

The effects of assumed parameter values on computed response

Subsequent applications of sensitivity include

- Reliability analysis
  - Quantify system performance under multiple limit state
- Optimization
  - Find best solution for some objective functions and constraints on the system
- System identification
  - Inverse modeling, find model parameters that match observed results
- and others ...

Simply speaking, a sensitivity is a gradient,

$$\frac{\partial U}{\partial \theta}(x, y, z, t)$$

where,

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$$\frac{\partial U}{\partial \theta}(x, y, z, t)$$

where,

• U – response velocity, pressure, ...

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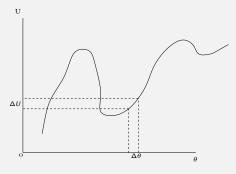
$$\frac{\partial U}{\partial \theta}(x, y, z, t)$$

where,

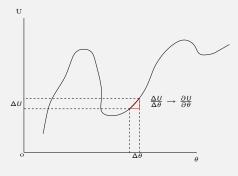
- U response velocity, pressure, ...
- $\theta$  modeling or physical property

• A simple way (Finite Difference Method)

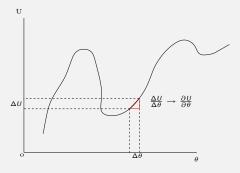
• A simple way (Finite Difference Method)



• A simple way (Finite Difference Method)

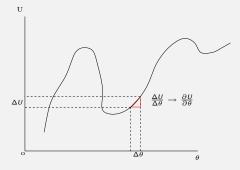


A simple way (Finite Difference Method)



- Require to solve response equations one more time for each parameter
- ullet Prone to round-off error for small  $\Delta heta$

A simple way (Finite Difference Method)



- Require to solve response equations one more time for each parameter
- ullet Prone to round-off error for small  $\Delta heta$

FDM is not practical due to the computational cost

$$M\dot{U} + KU = F$$

$$\begin{split} \mathbf{M}\dot{\mathbf{U}} + \mathbf{K}\mathbf{U} &= \mathbf{F} \\ \frac{\partial \mathbf{M}}{\partial \theta}\dot{\mathbf{U}} + \mathbf{M}\frac{\partial \dot{\mathbf{U}}}{\partial \theta} + \frac{\partial \mathbf{K}}{\partial \theta}\mathbf{U} + \mathbf{K}\frac{\partial \mathbf{U}}{\partial \theta} &= \frac{\partial \mathbf{F}}{\partial \theta} \end{split}$$

$$\begin{split} \mathbf{M}\dot{\mathbf{U}} + \mathbf{K}\mathbf{U} &= \mathbf{F} \\ \frac{\partial \mathbf{M}}{\partial \theta} \dot{\mathbf{U}} + \mathbf{M} \frac{\partial \dot{\mathbf{U}}}{\partial \theta} + \frac{\partial \mathbf{K}}{\partial \theta} \mathbf{U} + \mathbf{K} \frac{\partial \mathbf{U}}{\partial \theta} &= \frac{\partial \mathbf{F}}{\partial \theta} \\ \mathbf{M} \frac{\partial \dot{\mathbf{U}}}{\partial \theta} + \mathbf{K} \frac{\partial \mathbf{U}}{\partial \theta} &= \frac{\partial \mathbf{F}}{\partial \theta} - \frac{\partial \mathbf{M}}{\partial \theta} \dot{\mathbf{U}} - \frac{\partial \mathbf{K}}{\partial \theta} \mathbf{U} \end{split}$$

$$\begin{split} \mathbf{M}\dot{\mathbf{U}} + \mathbf{K}\mathbf{U} &= \mathbf{F} \\ \frac{\partial \mathbf{M}}{\partial \theta} \dot{\mathbf{U}} + \mathbf{M} \frac{\partial \dot{\mathbf{U}}}{\partial \theta} + \frac{\partial \mathbf{K}}{\partial \theta} \mathbf{U} + \mathbf{K} \frac{\partial \mathbf{U}}{\partial \theta} &= \frac{\partial \mathbf{F}}{\partial \theta} \\ \mathbf{M} \frac{\partial \dot{\mathbf{U}}}{\partial \theta} + \mathbf{K} \frac{\partial \mathbf{U}}{\partial \theta} &= \frac{\partial \mathbf{F}}{\partial \theta} - \frac{\partial \mathbf{M}}{\partial \theta} \dot{\mathbf{U}} - \frac{\partial \mathbf{K}}{\partial \theta} \mathbf{U} \end{split}$$

A direct way (Direct Differentiation Method – DDM)

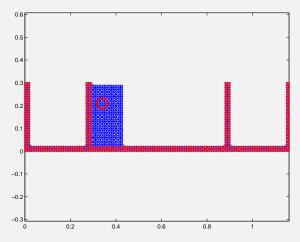
$$\begin{split} \mathbf{M}\dot{\mathbf{U}} + \mathbf{K}\mathbf{U} &= \mathbf{F} \\ \frac{\partial \mathbf{M}}{\partial \theta}\dot{\mathbf{U}} + \mathbf{M}\frac{\partial \dot{\mathbf{U}}}{\partial \theta} + \frac{\partial \mathbf{K}}{\partial \theta}\mathbf{U} + \mathbf{K}\frac{\partial \mathbf{U}}{\partial \theta} &= \frac{\partial \mathbf{F}}{\partial \theta} \\ \mathbf{M}\frac{\partial \dot{\mathbf{U}}}{\partial \theta} + \mathbf{K}\frac{\partial \mathbf{U}}{\partial \theta} &= \frac{\partial \mathbf{F}}{\partial \theta} - \frac{\partial \mathbf{M}}{\partial \theta}\dot{\mathbf{U}} - \frac{\partial \mathbf{K}}{\partial \theta}\mathbf{U} \\ &= \frac{\partial \mathbf{F}}{\partial \theta} - \frac{\partial \mathbf{M}}{\partial \theta}\dot{\mathbf{U}} - \frac{\partial \mathbf{K}}{\partial \theta}\mathbf{U} \end{split}$$

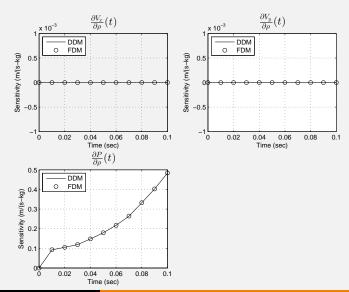
where,

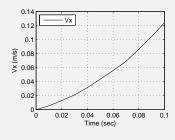
is the sensitivity "force" vector

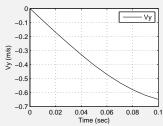
- Only form RHS vectors and solve linear equations once for each parameter, LHS matrices don't change,
- No additional round-off error as the FDM

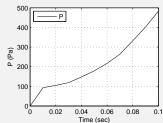
• Find  $\frac{\partial V_x}{\partial \rho}(t)$ ,  $\frac{\partial V_y}{\partial \rho}(t)$ ,  $\frac{\partial P}{\partial \rho}(t)$  for particle 400, the sensitivity of velocities and pressure to the density of the fluid.



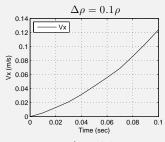


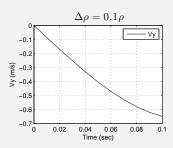


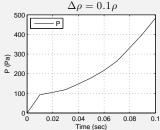




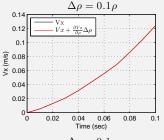
#### Example of sensitivity analysis

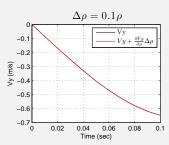


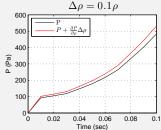




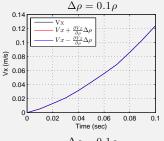
#### Example of sensitivity analysis

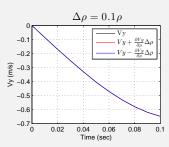


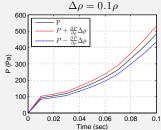


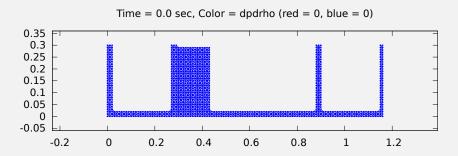


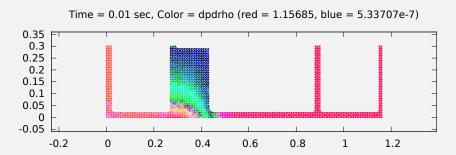
#### Example of sensitivity analysis

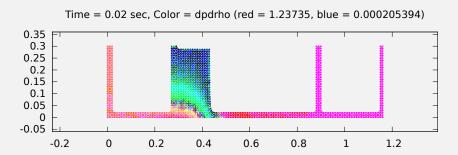


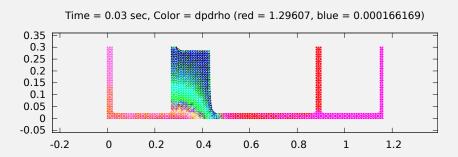


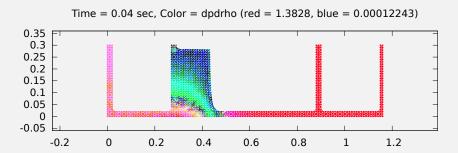


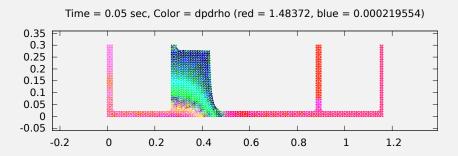


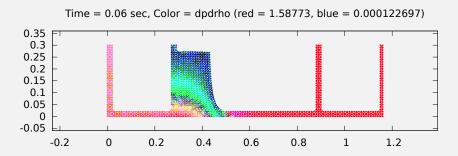


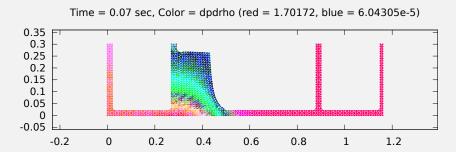


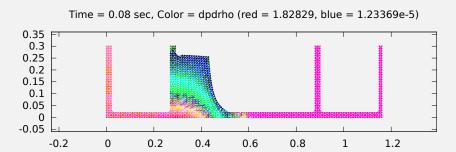


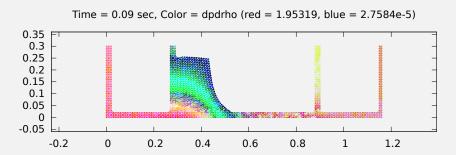


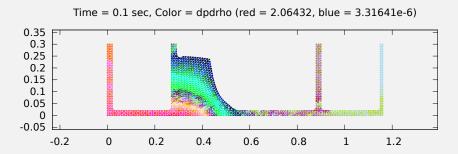


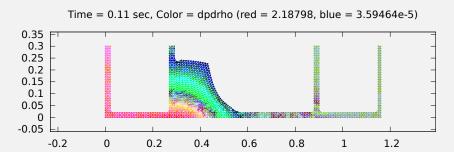


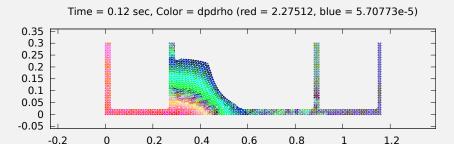


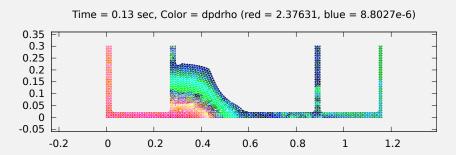


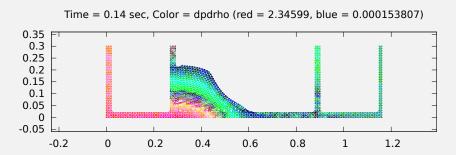


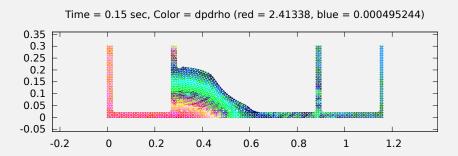


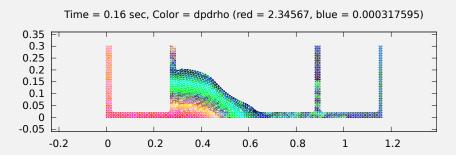


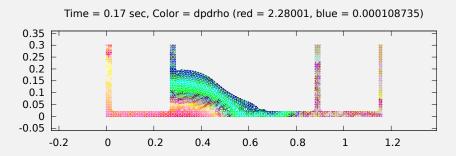


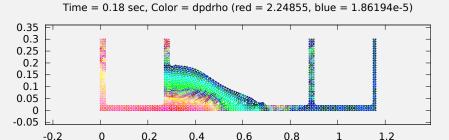


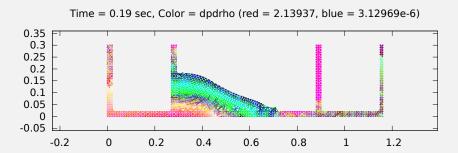


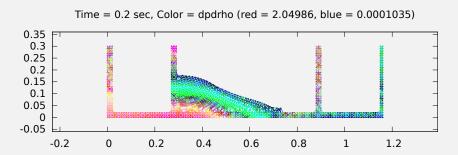


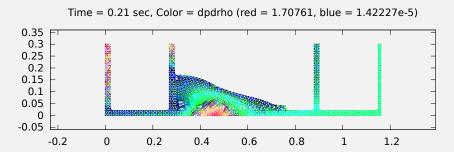


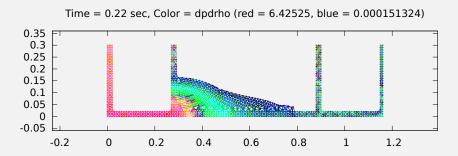


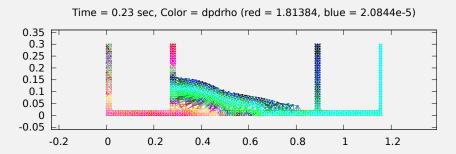


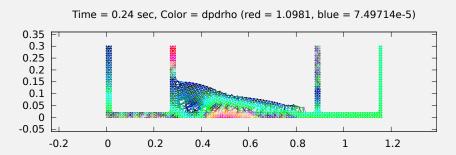


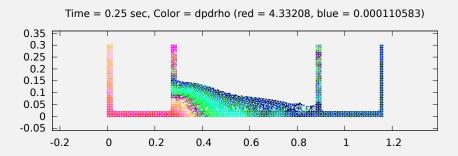


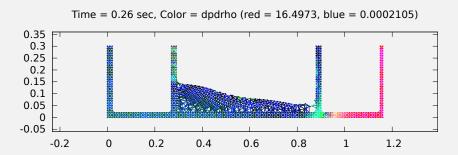


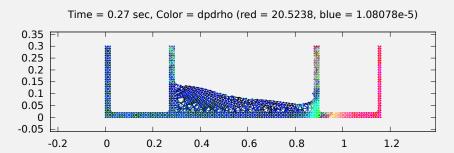


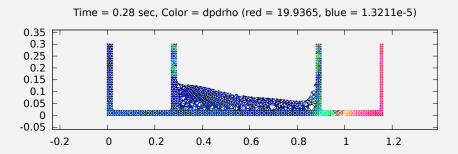


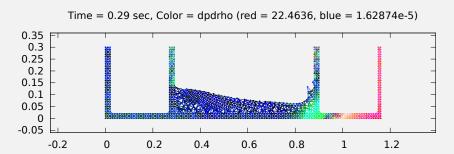


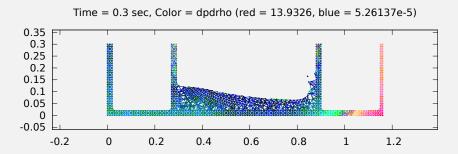


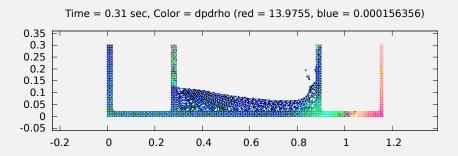


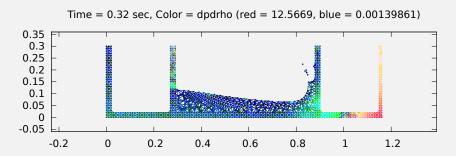


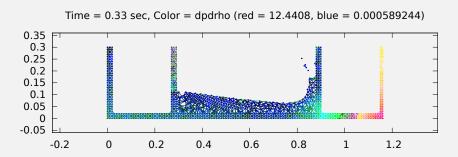


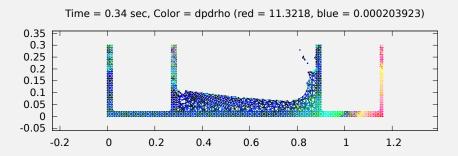


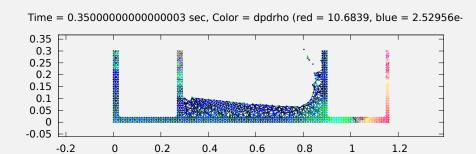


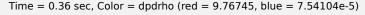


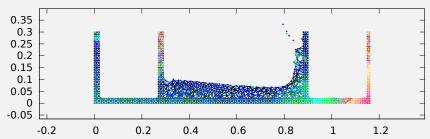




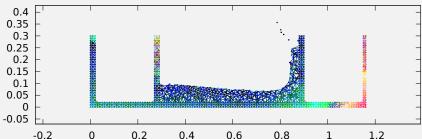


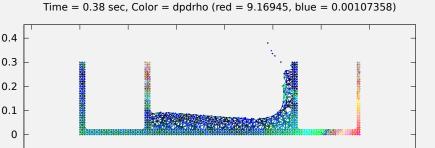












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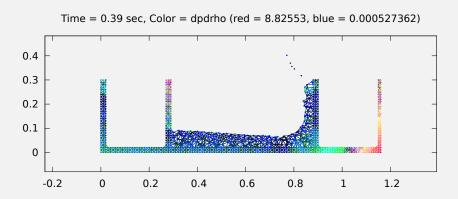
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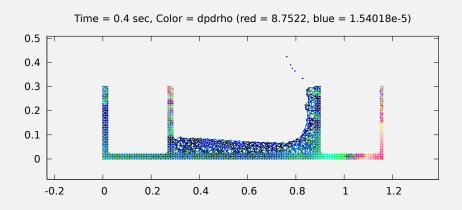
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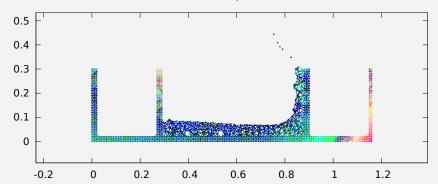
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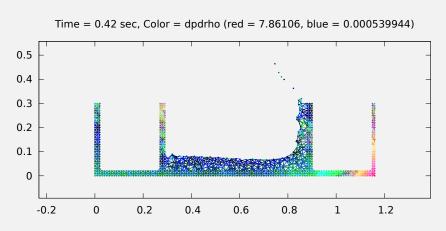
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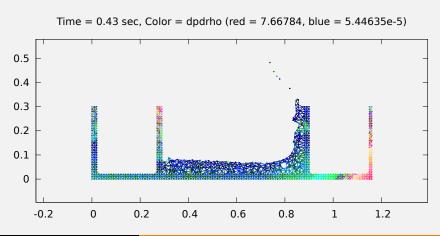


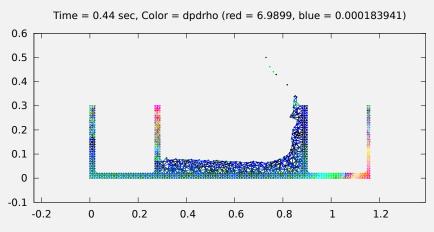


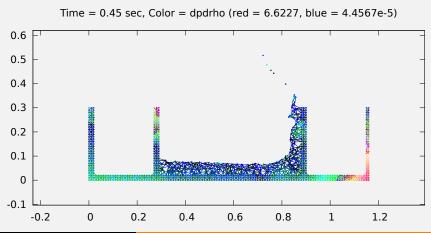
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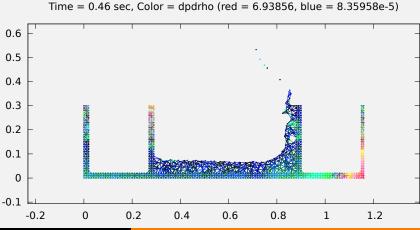


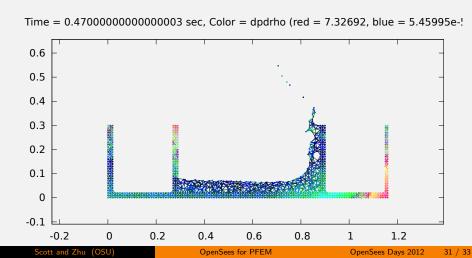


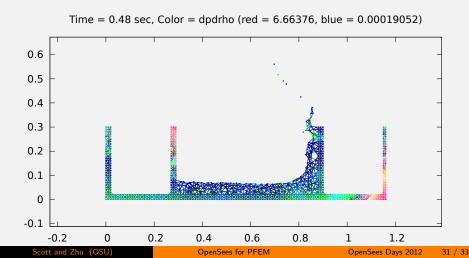


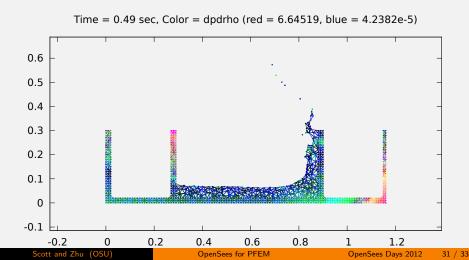


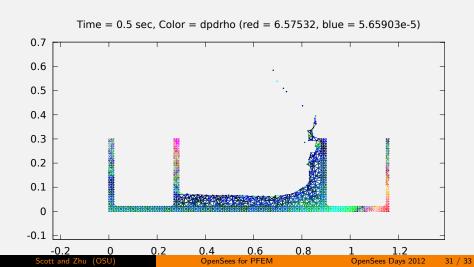


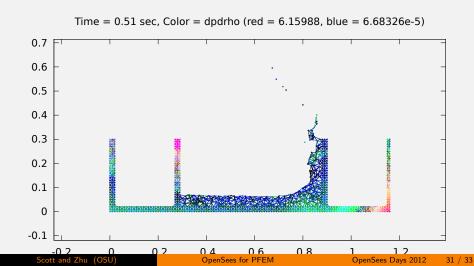


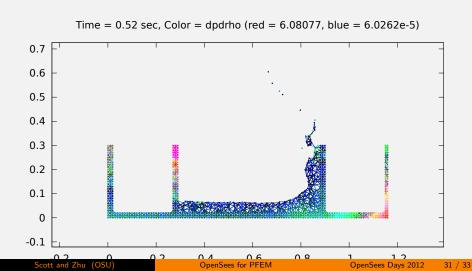


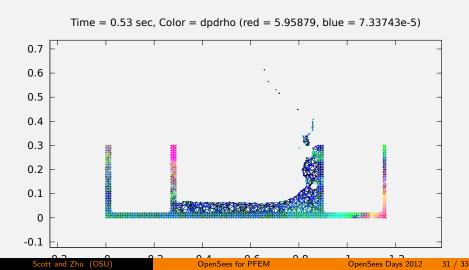


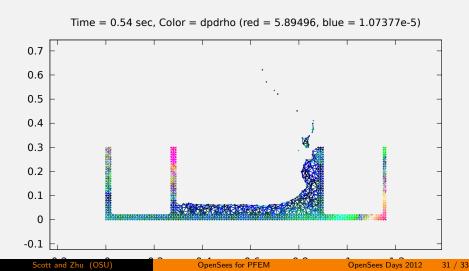


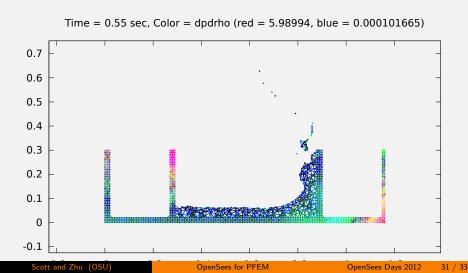


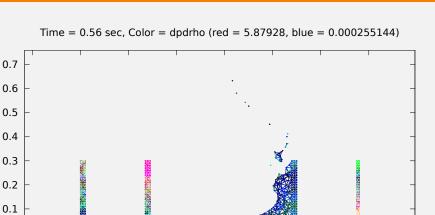






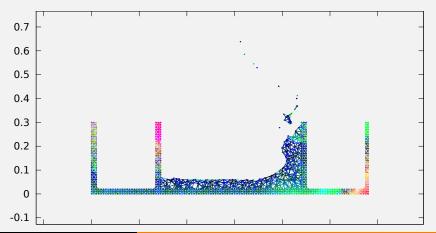


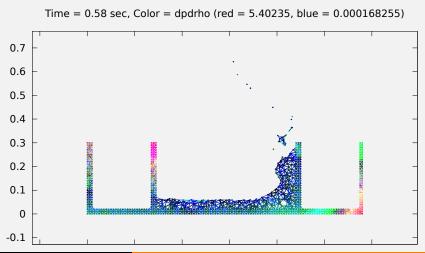


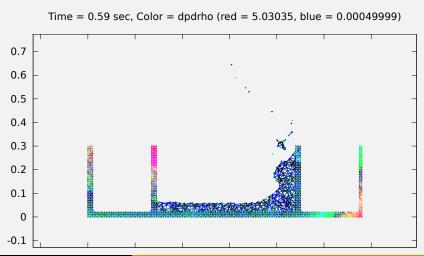


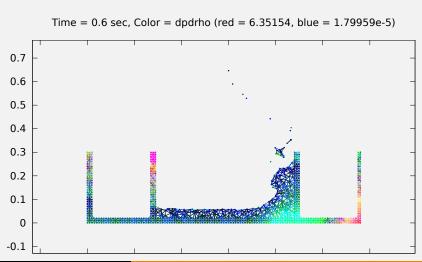
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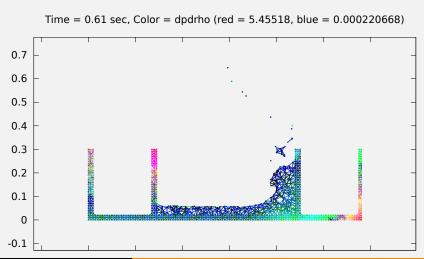
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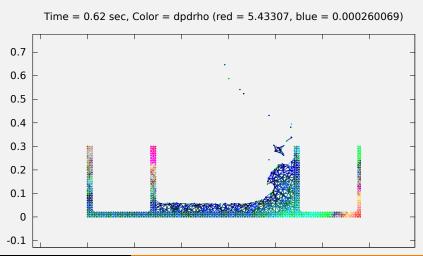


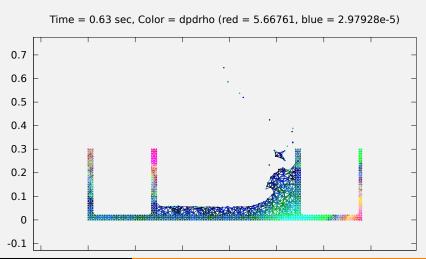


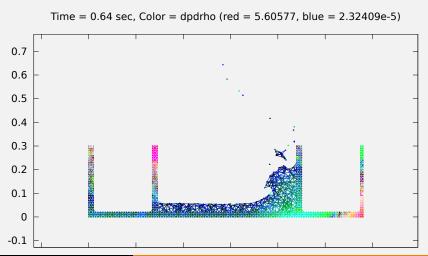


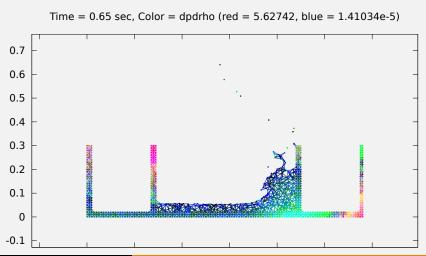


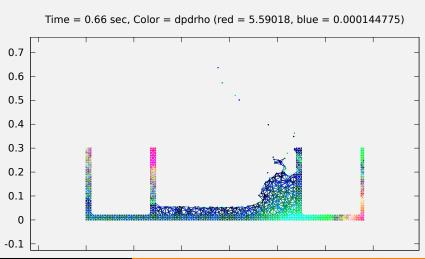




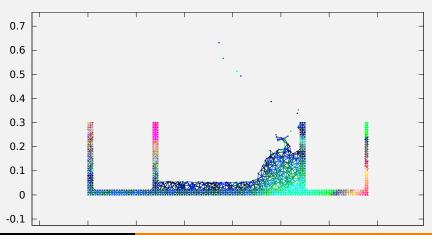


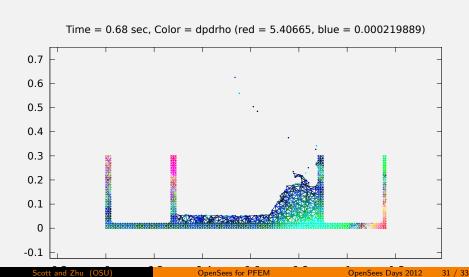


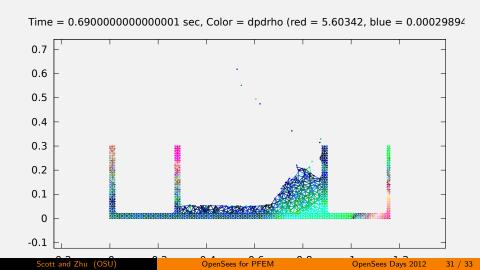


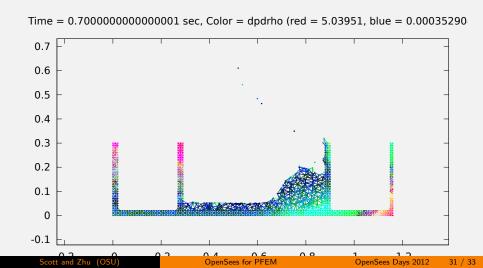


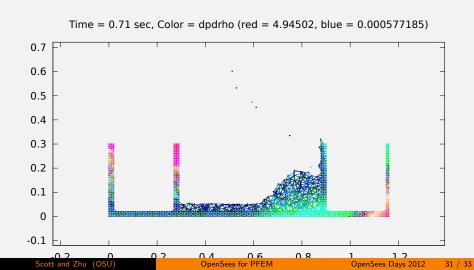
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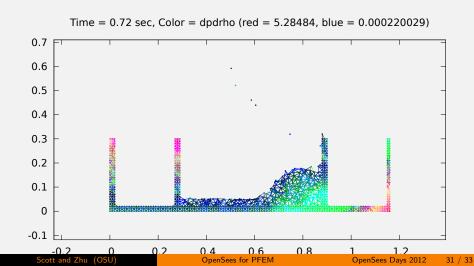


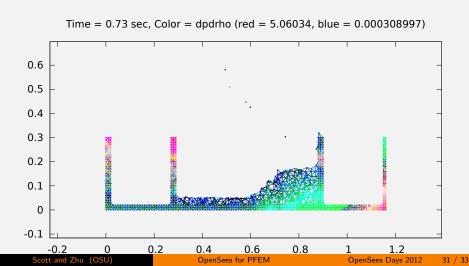


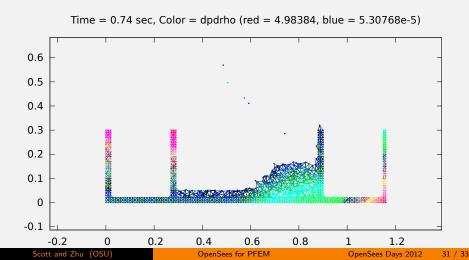


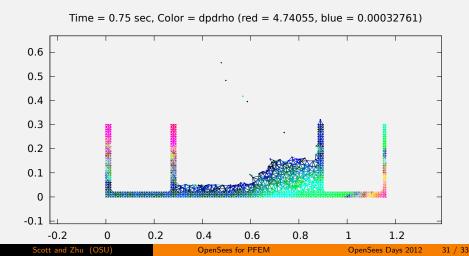


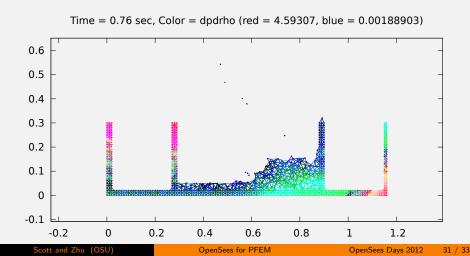


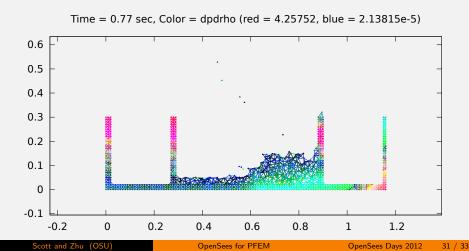


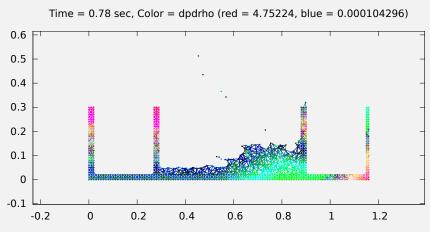


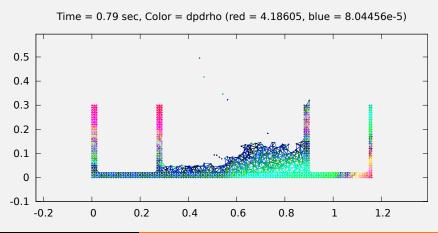


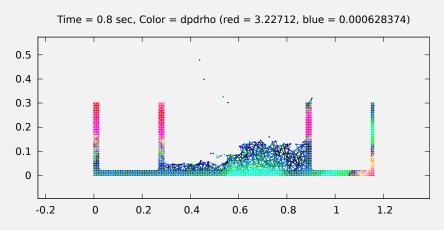


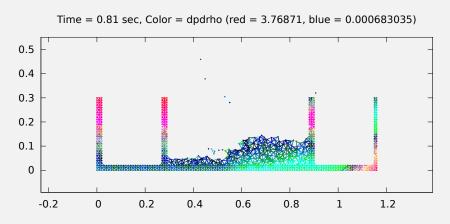


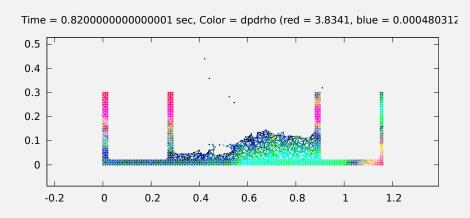


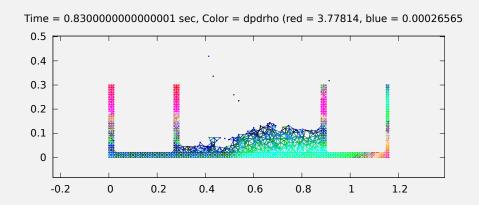


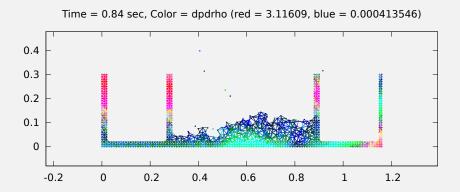


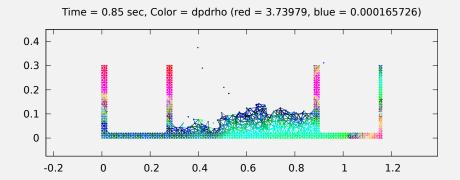


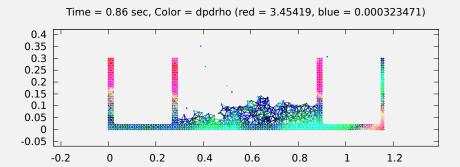


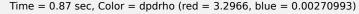


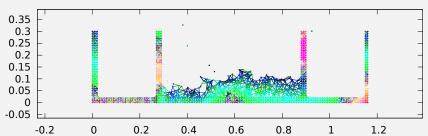




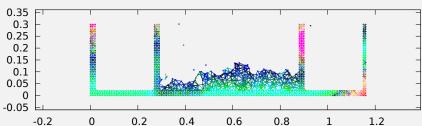


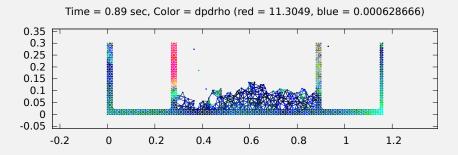


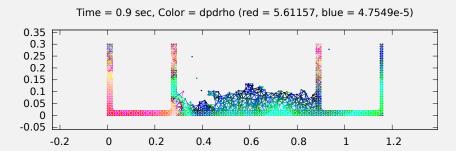


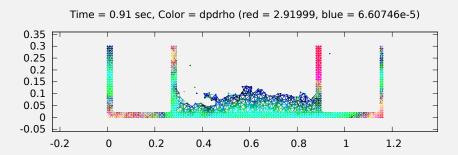


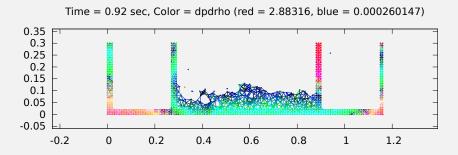


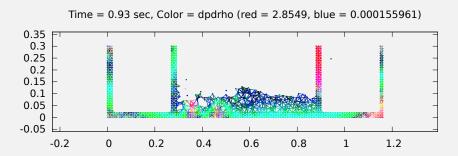


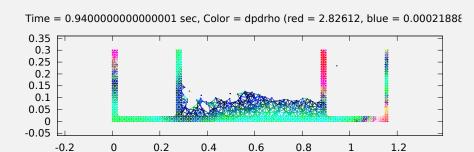


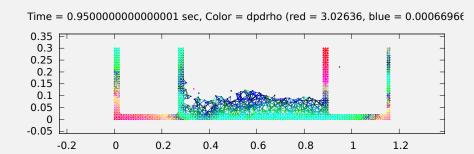


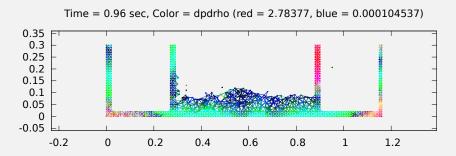


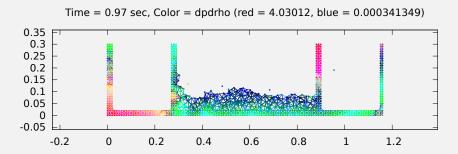


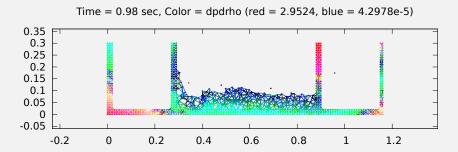


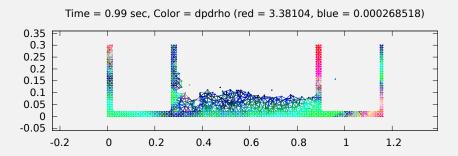












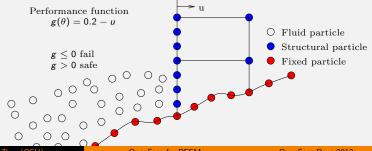
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Questions?