



Geotechnical Examples using OpenSees

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Outline

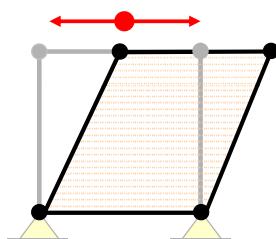
- **Take Advantage of tcl scripting!!**
 - Simple example
 - Push over pile analysis
 - Layout of more advance scripts for:
 - Push-over pile analysis
 - free-field analysis in liquefiable soils
 - Useful links
- **Take advantage of pre- and post- processors**
 - GID, just one possible alternative ☺
 - Dynamic analysis of piles
 - Analysis of complete bridge system
 - 3D analysis of piles

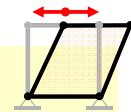
Take advantage of **tcl** scripting!!

- **tcl** can be used to develop scripts for geotechnical applications.
- Possible applications:
 - Pushover analysis (p-y) including nonlinear pile response – (similar to **Ipile**)
 - Free-field analysis (including liquefiable soil conditions)- (similar to **shake**)
 - Pile load tests
 - Consolidation
 - Dynamic analysis of piles
 - Other

Basic Example

- Response of saturated soil element to harmonic excitation



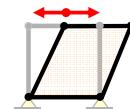


```

#Created by Zhaohui Yang (zhyang@ucsd.edu)
#plastic pressure dependent material
#plane strain, single element, dynamic analysis (input motion: sinusoidal acceleration at base)
#SI units (m, s, KN, ton)
#
#      4   3
#      -----
#      |   |
#      |   |
#      1-----2 (nodes 1 and 2 fixed)
#      ^   ^
#      <--> input motion: sinusoidal acceleration at base
wipe
#
#some user defined variables
#
set accMul 2      ;# acceleration multiplier
set massDen 2.0   ;# solid mass density
set fluidDen 1.0  ;# fluid mass density
set massProportionalDamping 0.0 ;
set stiffnessProportionalDamping 0.001 ;
set fangle 31.40  ;#friction angle
set ptangle 26.50  ;#phase transformation angle
set E 90000.0     ;#shear modulus
set poisson 0.40 ;
set G [expr $E/(2*(1+$poisson))] ;
set B [expr $E/(3*(1-2*$poisson))] ;
set press 0.0 ;# isotropic consolidation pressure on quad element(s)
set deltaT 0.010 ;# time step for analysis
set numSteps 2000 ;# Number of analysis steps
set gamma 0.600 ;# Newmark integration parameter
set period 1 ;# Period of applied sinusoidal load
set pi 3.1415926535 ;
set inclination 0 .
set unitWeightX [expr ($massDen-$fluidDen)*9.81*sin($inclination/180.0*$pi)] ;# unit weight in X direction
set unitWeightY [expr -($massDen-$fluidDen)*9.81*cos($inclination/180.0*$pi)] ;# unit weight in Y direction

```

Define basic variables using good names!!!



Define model geometry, materials & fixities

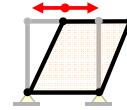
```

#####
#####
# create the ModelBuilder
model basic -ndm 2 -ndf 2
#####
#
# define material and properties
nDMaterial PressureDependMultiYield 2 2 $massDen $G $B $fangle .1 80 0.5 \
$ptangle 0.17 0.4 10 10 0.015 1.0
nDMaterial FluidSolidPorous 1 2 2 2.2D+6
updateMaterialStage -material 1 -stage 0
updateMaterialStage -material 2 -stage 0
#
# define the nodes
node 1 0.0D0 0.0D0
node 2 1.0D0 0.0D0
node 3 1.0D0 1.0D0
node 4 0.0D0 1.0D0
#
# define the element thick material maTag press mDensity gravity
element quad 1 1 2 3 4 1.0 "PlaneStrain" 1 $press 0. $unitWeightX $unitWeightY
#
# fix the base
fix 1 1 1
fix 2 1 1
#
#tie nodes 3 and 4
equalDOF 3 4 1 2

```

Define gravity step

VERY IMPORTANT!!!



```
#####
# GRAVITY APPLICATION (plastic behavior)
#
# create the SOE, ConstraintHandler, Integrator, Algorithm and Numberer
system ProfileSPD
test NormDispIncr 1.D-12 25 0
constraints Transformation
integrator LoadControl 1 1 1
algorithm Newton
numberer RCM

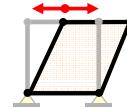
#
# create the Analysis
analysis Static

#
#analyze
analyze 2

#
# switch the material to plastic
updateMaterialStage -material 1 -stage 1
updateMaterialStage -material 2 -stage 1
updateParameter -material 2 -refB [expr $G*2/3.];

#
#analyze
analyze 1
```

Define dynamic step



```
#####
# NOW APPLY LOADING SEQUENCE AND ANALYZE (plastic)

#
# rezero time
setTime 0.0
wipeAnalysis

#
#create loading pattern
pattern UniformExcitation 1 1 -accel "Sine 0 1000 $period -factor $accMul"

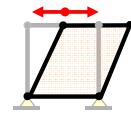
#
# create the Analysis
constraints Transformation;
test NormDispIncr 1.D-12 25 0
algorithm Newton
numberer RCM
system ProfileSPD
Integrator Newmark $gamma [expr pow($gamma+0.5, 2)/4] \
    $massProportionalDamping 0.0 $stiffnessProportionalDamping 0.0
analysis VariableTransient

#
#create Recorders
recorder Node -file disp.out -time -node 1 2 3 4 -dof 1 2 -dT 0.01 disp
recorder Node -file acce.out -time -node 1 2 3 4 -dof 1 2 -dT 0.01 accel
recorder Element -ele 1 -time -file stress1.out material 1 stress -dT 0.01
recorder Element -ele 1 -time -file strain1.out material 1 strain -dT 0.01
recorder Element -ele 1 -time -file stress3.out material 3 stress -dT 0.01
recorder Element -ele 1 -time -file strain3.out material 3 strain -dT 0.01
recorder Element -ele 1 -time -file press1.out material 1 pressure -dT 0.01
recorder Element -ele 1 -time -file press3.out material 3 pressure -dT 0.01

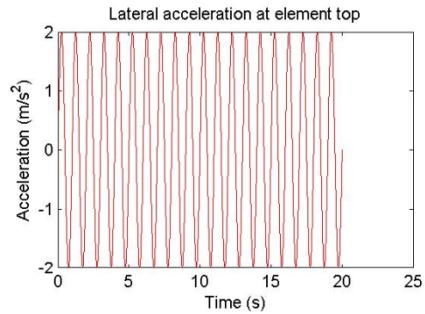
#
#analyze
set startT [clock seconds]
analyze $numSteps $deltaT [expr $deltaT/100] $deltaT 10
set endT [clock seconds]
puts "Execution time: [expr $endT-$startT] seconds."

#
wipe #flush ouput stream
```

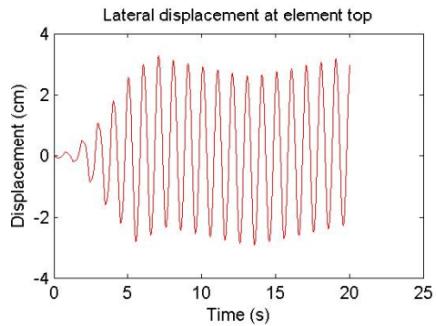
Plot Results



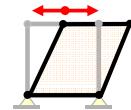
Input Accel time history



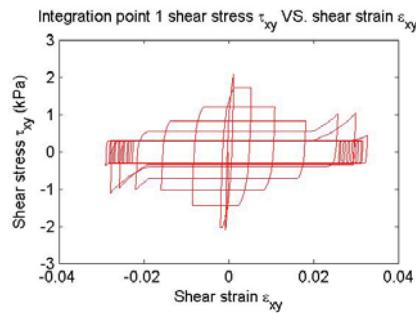
Output displ. time history



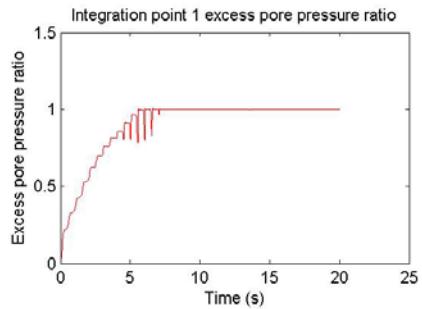
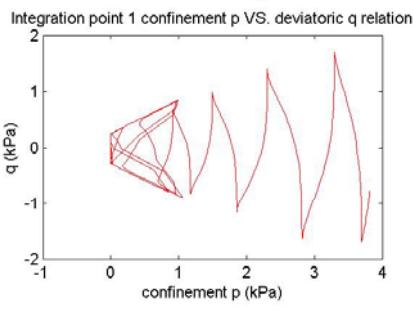
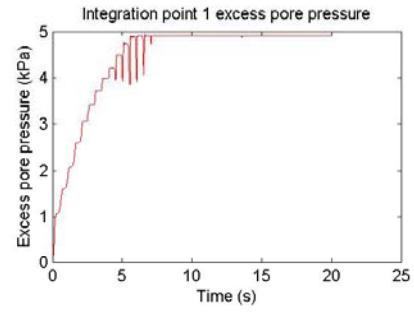
Plot results



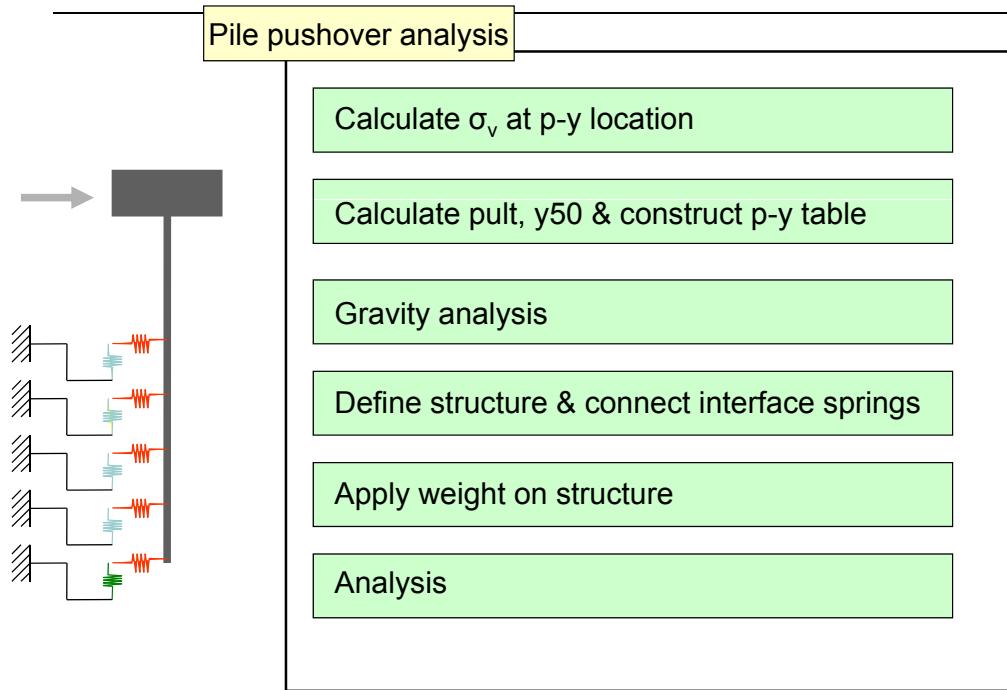
Stress-strain & stress path



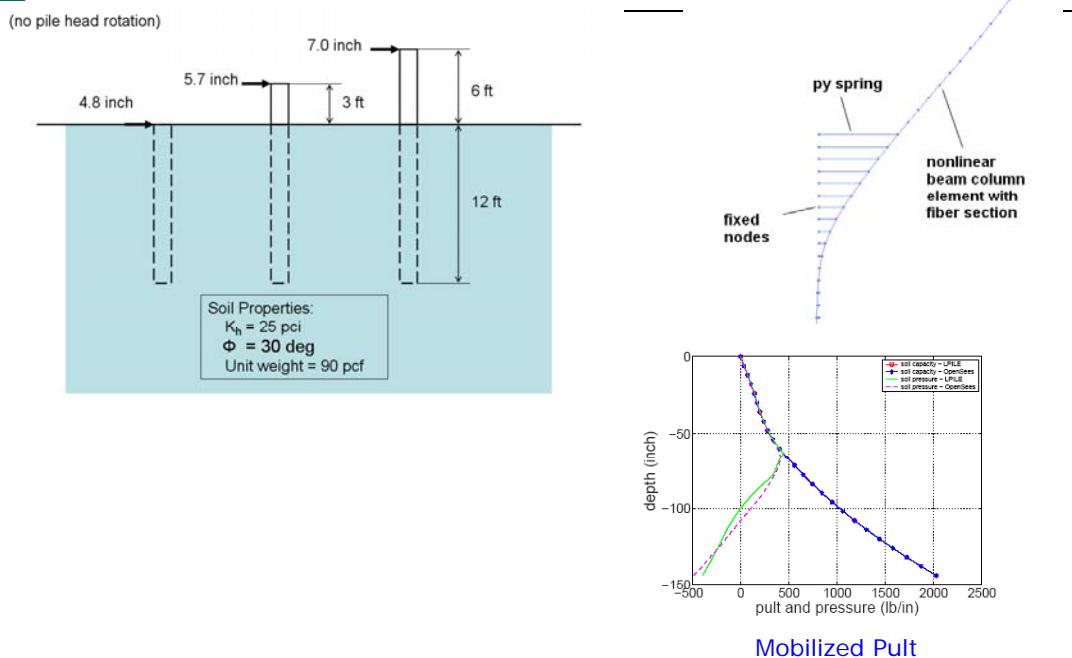
Pore pressures



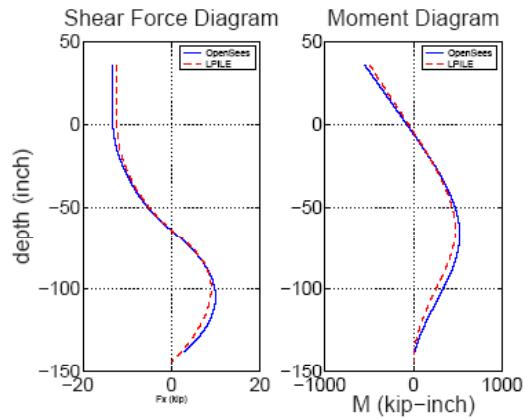
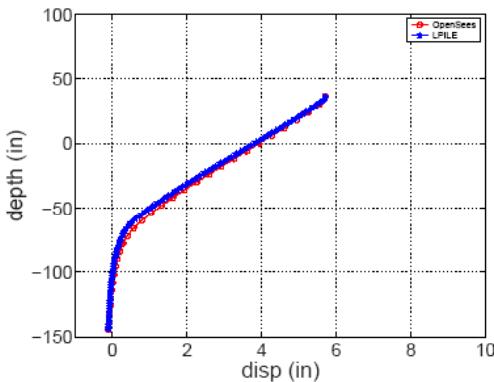
Pushover Pile Analysis using OpenSees



Pushover Pile Analysis using OpenSees



Pushover Pile Analysis using OpenSees



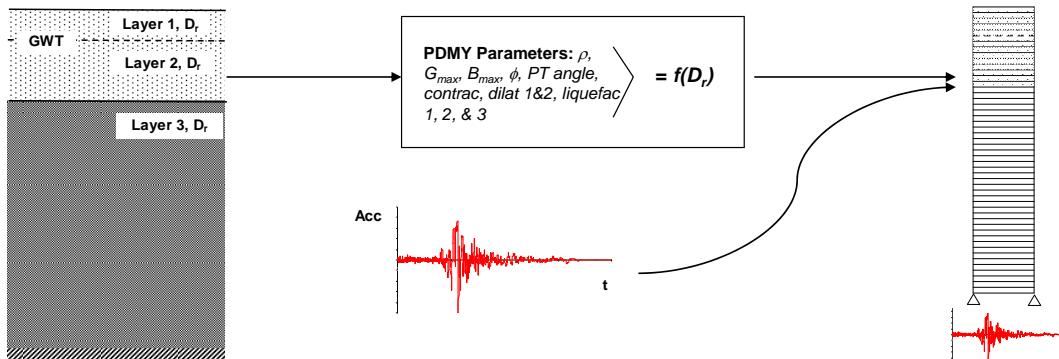
Free-Field Liquefaction Analysis using OpenSees

Profile information – layer depths, GWT depth, Dr for each layer, and # of elements per layer → ***openShakeV5.tcl***

Input acceleration time histories – file name, Dt, and # steps → ***earthquakeV5.tcl***

PDMDYparametersV5.tcl computes material parameters for each layer based on Dr and position w.r.t. GWT

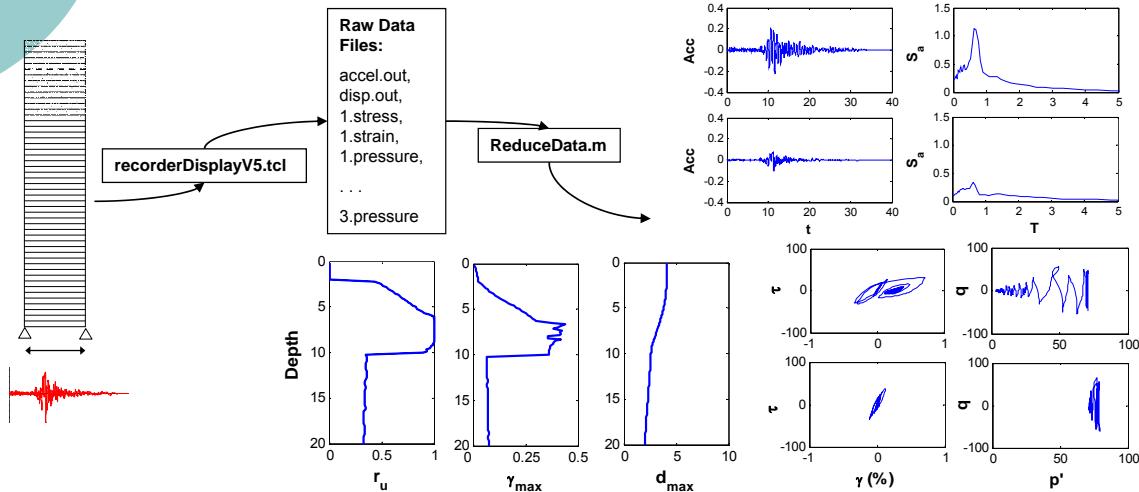
openShakeAnalysisV5.tcl builds nodal mesh, defines layer materials based on PDMDY parameters, applies input acceleration to profile base, and performs dynamic analysis



Free-Field Liquefaction Analysis using OpenSees (cont.)

recorderDisplayV5.tcl records nodal accelerations and displacements and elemental stresses, strains, and excess porepressures for each analysis time step. Data is saved to files organized by layer and data type

ReduceData.m organizes the data into arrays and produces plots of analysis Results at user-specified locations in the profile



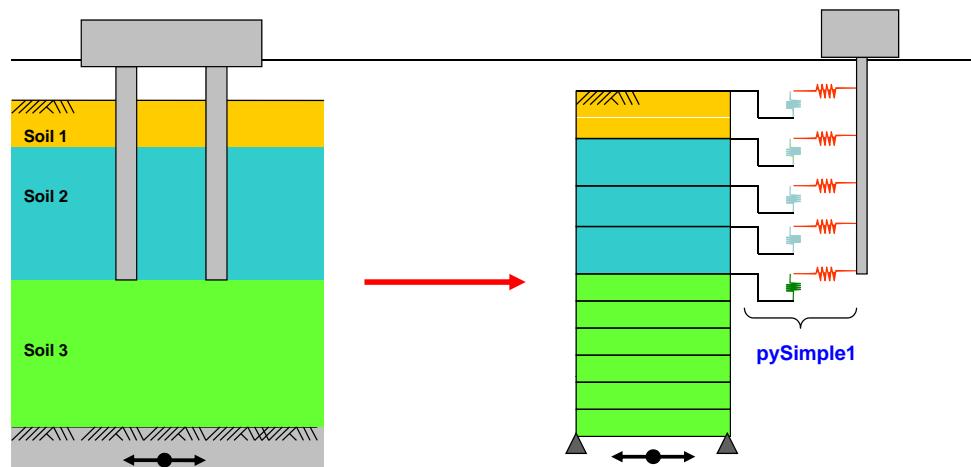
Other useful tcl scripts @

- <http://opensees.berkeley.edu/>
- <http://sokocalo.engr.ucdavis.edu/~jeremic>
- <http://cyclic.ucsd.edu/opensees/>
- http://www.ce.washington.edu/~geotech/opensees/PEER/davis_meeting/

Take advantage of pre- and post-processors

- Difficult to create **tcl** scripts for complex boundary value geotechnical problems.
 - complex foundation configurations
 - embankments
 - wharves
 - bridges
 - 3-D analysis
- Need to use pre- and post processors to create meshes and visualize results
- **GID**, just one possible alternative ☺

Dynamic Analysis of Piles in OpenSees



Soil → quad / up94 quad element

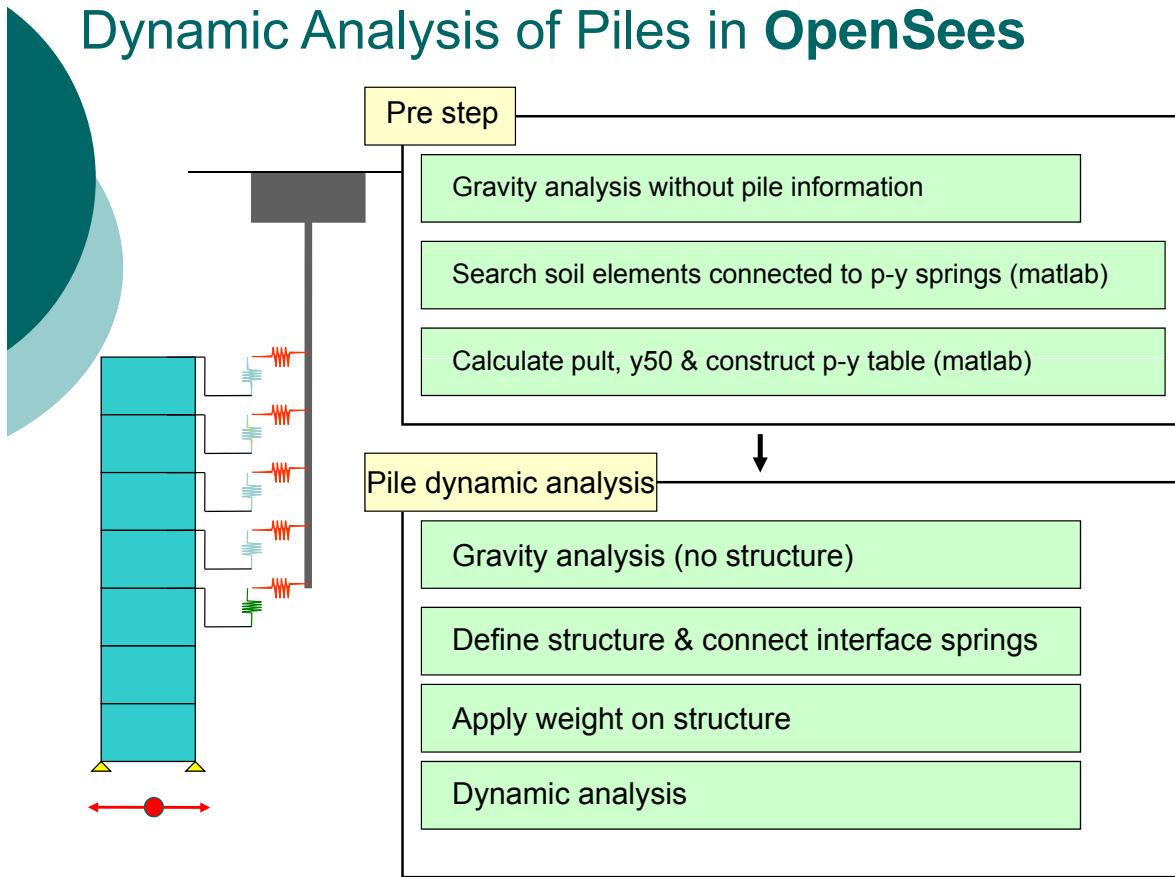
PDMY material (+ FluidSolidPorous Material)

Pile → elastic / nonlinear beam column element

Interaction → zeroLength element

pySimple1, tzSimple1, qzSimple1, or liquefiable p-y

Dynamic Analysis of Piles in OpenSees



Dynamic Analysis of Piles in OpenSees

```

#-----#
# Unit: m, s, kN
#-----#
model BasicBuilder -ndm 2 -ndf 2

# =====#
# (1) nodes (soil.py,dashpot,boundary,zeronode)
# =====#
node 1 0.0000000000 0.0000000000
node 2 0.0000000000 0.5200000000
node 3 0.0000000000 1.0400000000
...
node 569 93.4180000000 27.3000000000
node 570 93.4180000000 27.5600000000
node 571 93.4180000000 27.8200000000

# =====#
# (2) define nDMaterial for soil
# =====#
nDMaterial PressureDependMultiYield 51 2 1.66 100000.0 300000.0 37.000 0.100 80.000 0.500 2
    updateMaterialStage -material 51 -stage 0
nDMaterial PressureDependMultiYield 52 2 1.66 100000.0 300000.0 37.000 0.100 80.000 0.500 2
    updateMaterialStage -material 52 -stage 0
nDMaterial PressureDependMultiYield 53 2 1.66 100000.0 300000.0 37.000 0.100 80.000 0.500 2
    updateMaterialStage -material 53 -stage 0

# =====#
# (3) define quadElement for soil (max-10 soils)
# =====#
element quad 1 251 254 75 74 $eleThick PlaneStrain $matID1 $p 1.66 $gX [expr $gY/(1/1.66)]
element quad 2 254 258 76 75 $eleThick PlaneStrain $matID1 $p 1.66 $gX [expr $gY/(1/1.66)]
element quad 3 258 261 77 76 $eleThick PlaneStrain $matID1 $p 1.66 $gX [expr $gY/(1/1.66)]
element quad 4 261 269 78 77 $eleThick PlaneStrain $matID1 $p 1.66 $gX [expr $gY/(1/1.66)]
...
element quad 160 265 264 492 493 $eleThick PlaneStrain $matID3 $p 1.66 $gX [expr $gY/(1/1.66)]
element quad 161 264 263 491 492 $eleThick PlaneStrain $matID3 $p 1.66 $gX [expr $gY/(1/1.66)]
element quad 162 263 262 490 491 $eleThick PlaneStrain $matID3 $p 1.66 $gX [expr $gY/(1/1.66)]

```

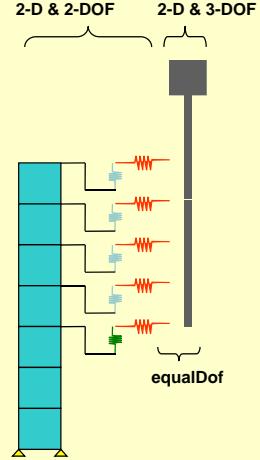
The diagram shows a pile system with two options for modeling: '2-D & 2-DOF' and '2-D & 3-DOF'. The '2-D & 2-DOF' option is shown on the left, where the pile is represented by a vertical stack of teal rectangular segments, each connected to a horizontal beam at its top. Small red spring elements are attached to the side of the pile, representing soil-pile interaction. A horizontal double-headed arrow at the base indicates lateral movement or displacement. The '2-D & 3-DOF' option is shown on the right, where the pile is represented by a vertical stack of teal rectangular segments, each connected to a horizontal beam at its top. Small red spring elements are attached to the side of the pile, representing soil-pile interaction. A horizontal double-headed arrow at the base indicates lateral movement or displacement. The '2-D & 3-DOF' option includes a green circle labeled 'equalDOF' at the base of the pile.

Dynamic Analysis of Piles in OpenSees

```

# =====#
# (4) define uniaxialMaterial for Py-Tz (imported data)
# =====#
set channel9 [open "./data/pult.dat" r] ;# pult imported
set ctr9 0;
foreach line9 [split [read -nonewline $channel9] \n] {
    set lineSize9 [llength $line9]
    set ctr9 [expr $ctr9+1];
    set lineData9($ctr9) $line9
    set lineNumber9 $ctr9
}
close $channel9
#-----
for {set i 1 } {$i <= $lineNumber9} {incr i 1} {
    for {set j 0 } {$j < $lineSize9} {incr j 1} {
        set data9($i,$j) [lindex $lineData9($i) $j]
    }
}
#-----
set kk0 0
for {set i 1 } {$i <= $lineNumber9} {incr i 1} {
    set kk0 [expr $kk0+1]
    set pyElement($kk0) [expr int($data9($i,0))]
    set connect1($kk0) [expr int($data9($i,1))]
    set connect2($kk0) [expr int($data9($i,2))]
    set y50($kk0) [expr int($data9($i,3))]
    set y50($kk0) $data9($i,4)
    set Cd($kk0) $data9($i,5)
    set tzType($kk0) [expr int($data9($i,6))]
    set z50($kk0) $data9($i,7)
    set pult($kk0) $data9($i,8)
    set tult($kk0) $data9($i,9)
    set pyTzQzIndex($kk0) $data9($i,11)
}
## =====#
# (5) define zeroLength element for Py-Tz & Qz
# =====#
for {set i 1 } {$i <= $lineNumber9} {incr i 1} {
    if {$pyTzQzIndex($i) == 1} {
        uniaxialMaterial PySimple1 [expr $i+400] $pyType($i) $pult($i) $y50($i) $Cd($i) 0.01
        uniaxialMaterial TzSimple1 [expr $i+600] $tzType($i) $tult($i) $z50($i) 0.01
        element zeroLength $pyElement($i) $connect1($i) $connect2($i) -mat [expr $i+400] [expr $i+600] -dir 1 2
    } else {
        uniaxialMaterial PySimple1 [expr $i+400] $pyType($i) $pult($i) $y50($i) $Cd($i) 0.01
        uniaxialMaterial OzSimple1 [expr $i+600] $tzType($i) $tult($i) $z50($i) 0.0 0.01
        element zeroLength $pyElement($i) $connect1($i) $connect2($i) -mat [expr $i+400] [expr $i+600] -dir 1 2
    }
}

```



Dynamic Analysis of Piles in OpenSees

```

# =====#
# (6) define equal DOF (soil to soil)
# =====#
equalDOF 2 84 1 2
equalDOF 3 85 1 2
equalDOF 4 86 1 2
...
equalDOF 470 568 1 2
equalDOF 472 569 1 2
equalDOF 475 570 1 2
equalDOF 479 571 1 2

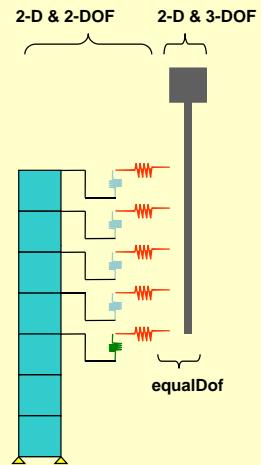
# =====#
# (7) define the fixity
# =====#
fix 1 1 1
fix 83 1 1
fix 262 1 1
fix 490 1 1

# =====#
# (8) create the analysis method & analyze
# =====#
system ProfileSPD
test NormDispIncr
algorithm Newton
constraints Transformation
integrator LoadControl 1 1 1
numberer Plain
analysis Static

analyze 1

# =====#
# (9) updateMaterialStage
# =====#
updateMaterialStage -material 51 -stage 1
updateMaterialStage -material 52 -stage 1
updateMaterialStage -material 53 -stage 1

```



Dynamic Analysis of Piles in OpenSees

```

model basic -ndm 2 -ndf 3

# =====#
# (10) define nodes and mass for pile
# =====#
node 110 42.900000 13.520000
node 113 42.900000 13.780000
...
node 488 50.518000 35.100000
node 489 52.429000 33.410000

# =====#
# (11) define nodes and mass for pile
# =====#
mass 110 0.09410 0.09410 0.09410
mass 113 0.09410 0.09410 0.09410
...
mass 486 0.59100 0.59100 0.59100
mass 487 328.60000 328.60000 328.60000

# =====#
# (12) define element and material for pile
# =====#
#--- elastic pile
geomTransf Linear 1
element elasticBeamColumn 163 334 388 21.09 68.95e6 20.08 1
element elasticBeamColumn 164 388 474 21.09 68.95e6 20.08 1
element elasticBeamColumn 165 474 487 21.09 68.95e6 20.08 1

#--- fiber section pile
set integration_points 5
set section_tag 1
set trans_tag 1
set alum_fy 1.3e5
set alum_E 6.89e7

uniaxialMaterial Steel01 941 $alum_fy $alum_E $alumHardening_ratio
section Fiber 1 {
    patch circ 941 $numSubDiv_circ $numSubDiv_rad $yCenter $zCenter $intRad $extRad $starAng $endAng ;# core concrete fibers
}

element nonlinearBeamColumn 169 486 485 $integration_points $section_tag $trans_tag
element nonlinearBeamColumn 170 485 484 $integration_points $section_tag $trans_tag
element nonlinearBeamColumn 171 484 483 $integration_points $section_tag $trans_tag
element nonlinearBeamColumn 172 483 482 $integration_points $section_tag $trans_tag

```

Dynamic Analysis of Piles in OpenSees

```

# =====#
# (13) define equal DOF (soil to pile)
# =====#
equalDOF 111 110 1 2
equalDOF 112 113 1 2
...
equalDOF 477 476 1 2
equalDOF 478 480 1 2

# =====#
# (14) settim and wipAnalysis
# =====#
wipAnalysis
loadConst -time 0.0

# =====#
# (15) apply the weight of structures
# =====#
set numStep_sWgt 100
pattern Plain 1 "Linear" {
    load 110 0.000000 [expr 0.094100 /(-1/9.81)/$numStep_sWgt] 0.000000
    load 113 0.000000 [expr 0.094100 /(-1/9.81)/$numStep_sWgt] 0.000000
    ...
    load 486 0.000000 [expr 0.591000 /(-1/9.81)/$numStep_sWgt] 0.000000
    load 487 0.000000 [expr 328.600000 /(-1/9.81)/$numStep_sWgt] 0.000000
}

# =====#
# (16) Recorder (selfWgt steps)
# =====#
recorder Node -file ./data/$f1/displacement_gStep.out -time -node all -dof 1 2 disp
recorder Element -file ./data/$f1/stress1_gStep.out -time -eleRange 1 162 material 1 stress

# =====#
# (17) analysis method
# =====#
constraints Penalty 1.0e12 1.0e12
test NormDispIncr 1e-6 10 0
algorithm Newton
numberer Plain
system ProfileSPD
integrator LoadControl 1 1 1 1
analysis Static

analyze $numStep_sWgt

```

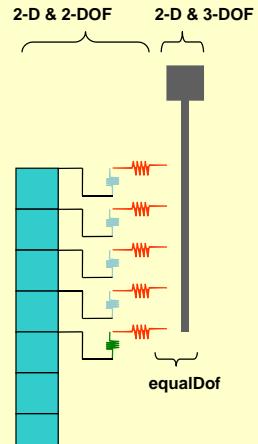
Dynamic Analysis of Piles in OpenSees

```
# =====#
# (18)   earthquake excitation
# =====#
wipeAnalysis
loadConst -time 0.0

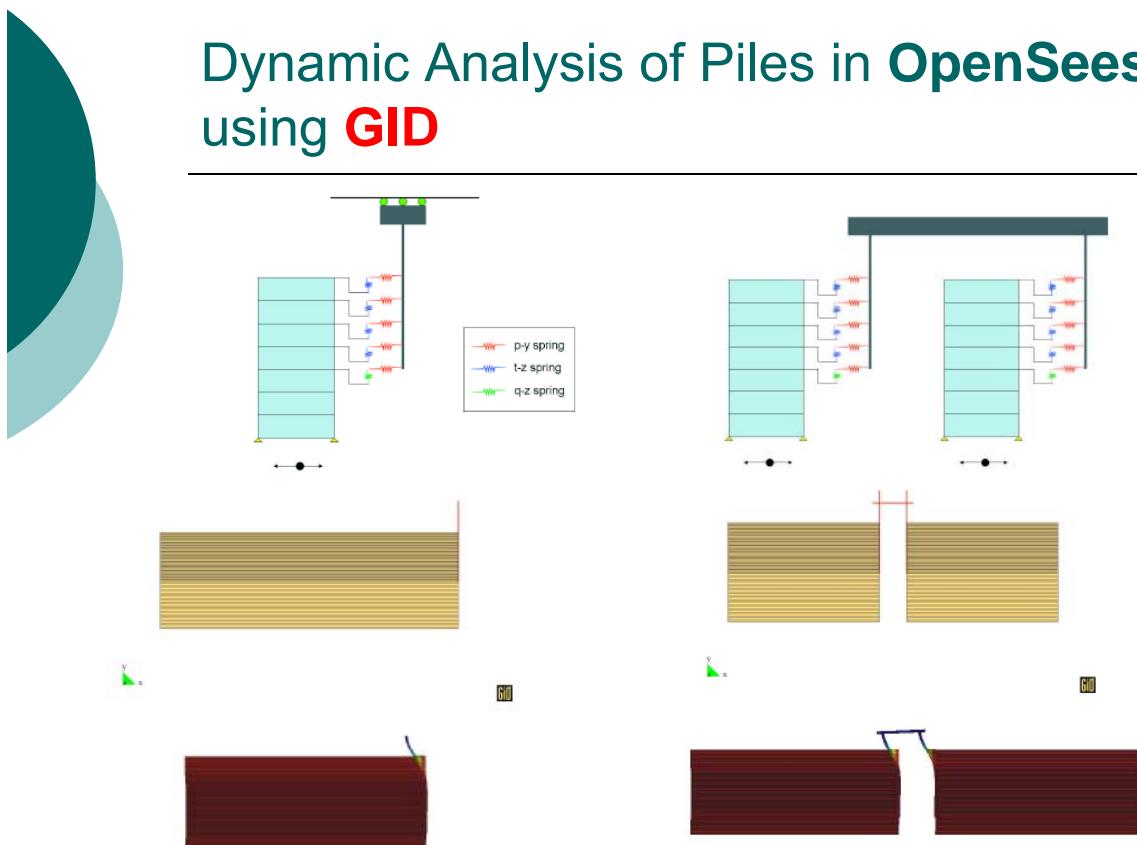
set accelSeries1 "Path -filePath ./OpenBaseMotions/CFG2_ax_base_02g_avg.txt -dt 0.0127 -factor 9.81"
pattern UniformExcitation 2 1 -accel $accelSeries1

# =====#
# (19)   recorder (earthquake step)
# =====#
remove recorders
recorder Node -file ./data/$f1/displacement.out -time -node all -dof 1 2 disp
recorder Node -file ./data/$f1/acceleration.out -time -node all -dof 1 2 accel
recorder Element -file ./data/$f1/pileForce.out -time -eleRange 163 292 force
recorder Element -file ./data/$f1/pyzDeformation.out -time -eleRange 293 404 deformation
recorder Element -file ./data/$f1/stress1.out -time -eleRange 1 162 material 1 stress
recorder Element -file ./data/$f1/stress2.out -time -eleRange 1 162 material 2 stress
recorder Element -file ./data/$f1/stress3.out -time -eleRange 1 162 material 3 stress
recorder Element -file ./data/$f1/stress4.out -time -eleRange 1 162 material 4 stress
recorder Element -file ./data/$f1/strain1.out -time -eleRange 1 162 material 1 strain
recorder Element -file ./data/$f1/strain2.out -time -eleRange 1 162 material 2 strain
recorder Element -file ./data/$f1/strain3.out -time -eleRange 1 162 material 3 strain
recorder Element -file ./data/$f1/strain4.out -time -eleRange 1 162 material 4 strain
recorder Element -file ./data/$f1/pressure1.out -time -eleRange 1 162 material 1 pressure
recorder Element -file ./data/$f1/pressure2.out -time -eleRange 1 162 material 2 pressure
recorder Element -file ./data/$f1/pressure3.out -time -eleRange 1 162 material 3 pressure
recorder Element -file ./data/$f1/pressure4.out -time -eleRange 1 162 material 4 pressure

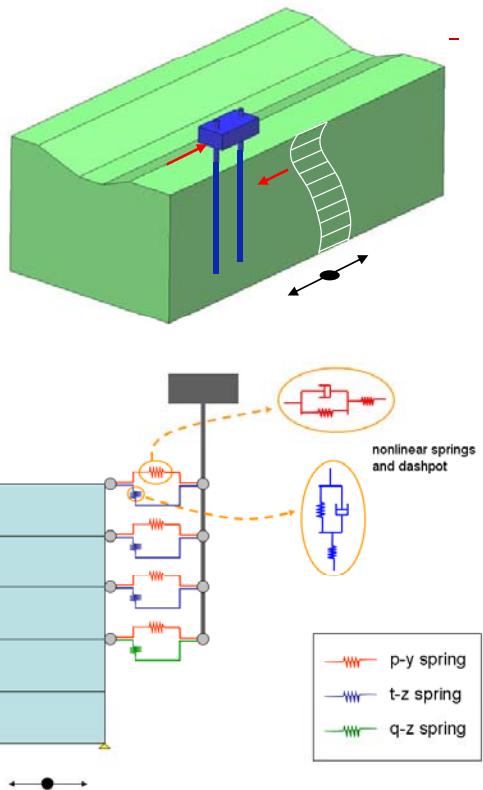
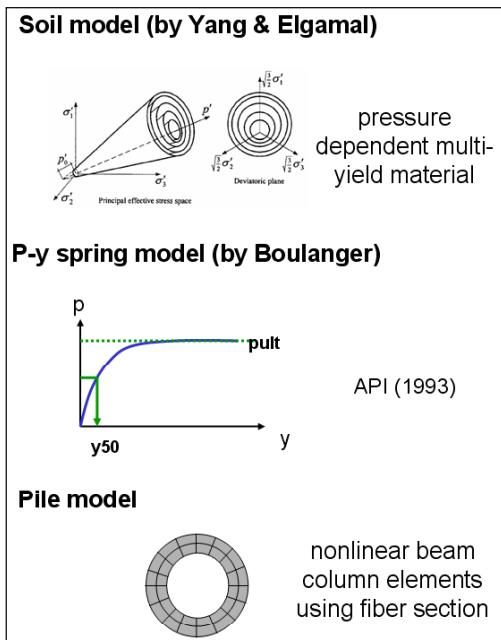
# =====#
# (20)           analysis method
# =====#
constraints Penalty 1.0e12 1.0e12
test NormDispIncr 1e-4 10 0
algorithm Newton
numberer Plain
system ProfileSPD
integrator Newmark 0.6 0.3025 0.0 0.0 0.001 0.0
analysis Transient
analyze 4096 0.0127
```



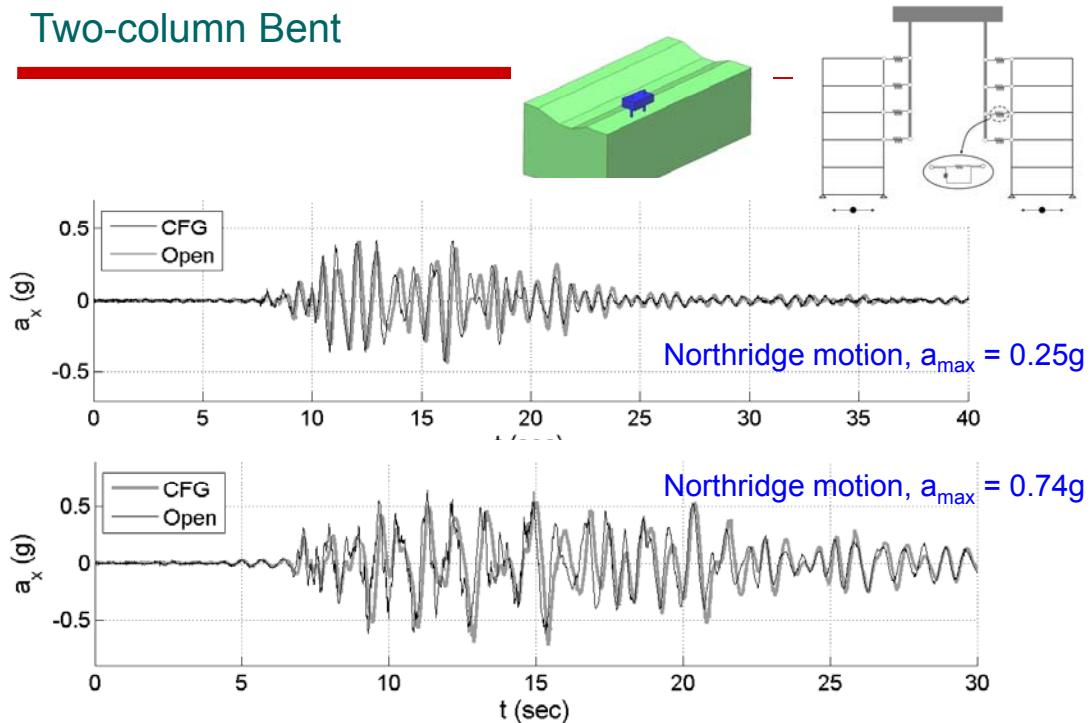
Dynamic Analysis of Piles in OpenSees using GID



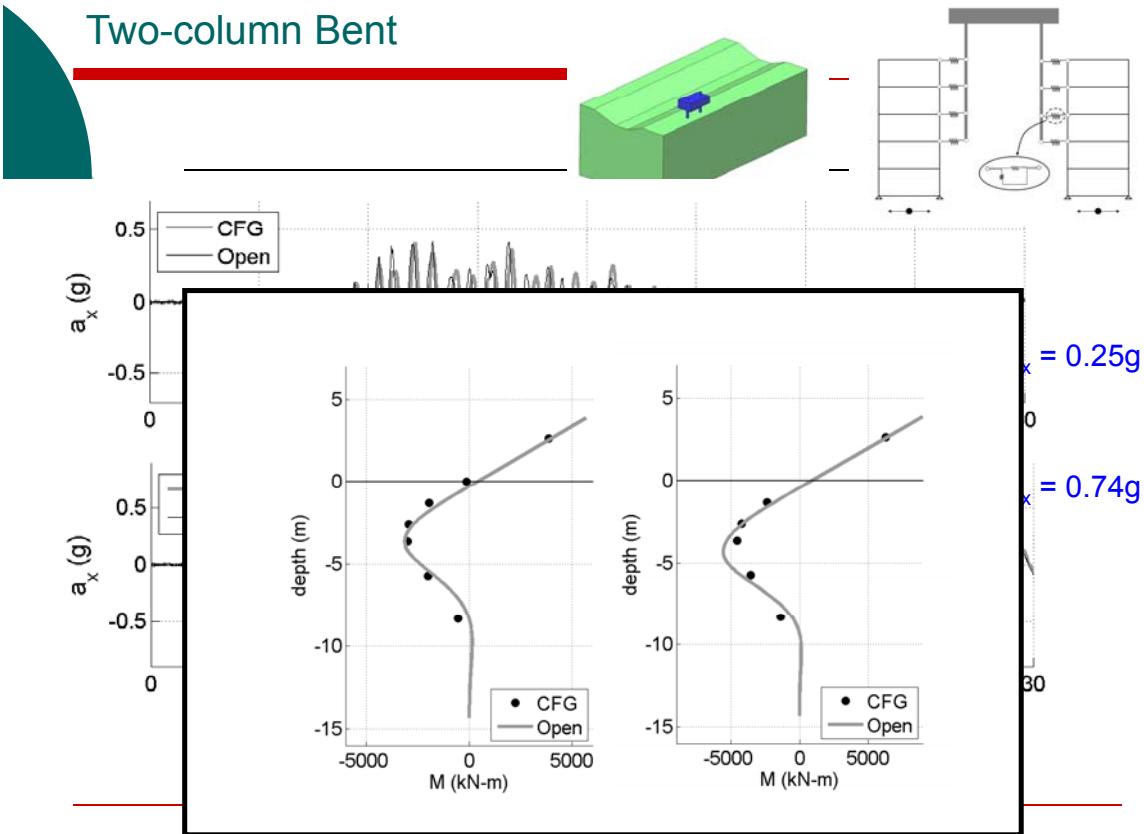
SPSI modeling in OpenSees



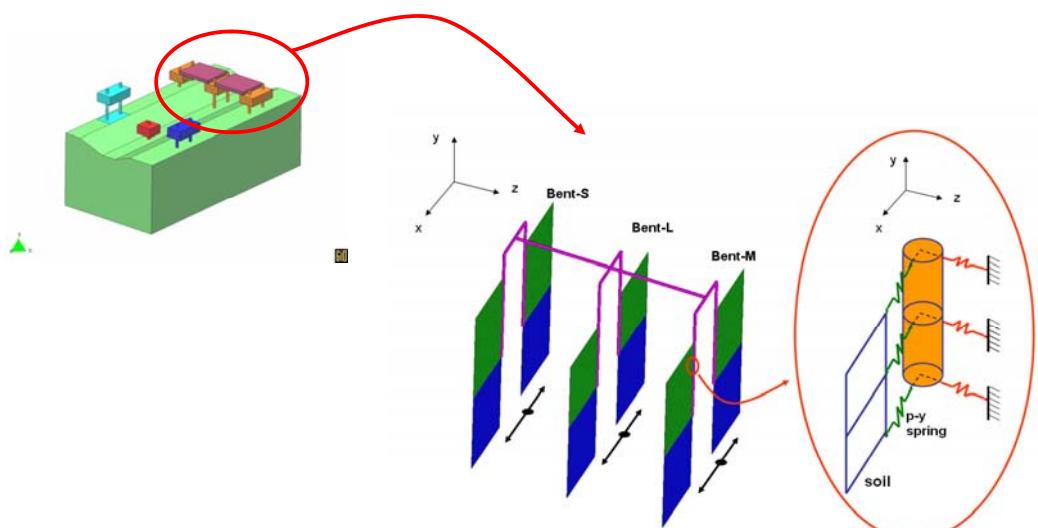
Two-column Bent



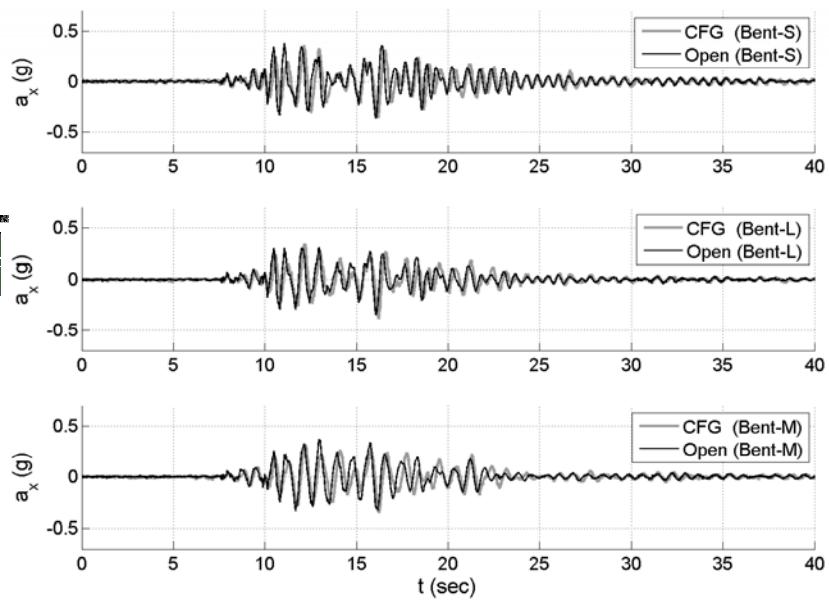
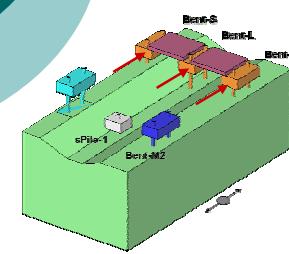
Two-column Bent



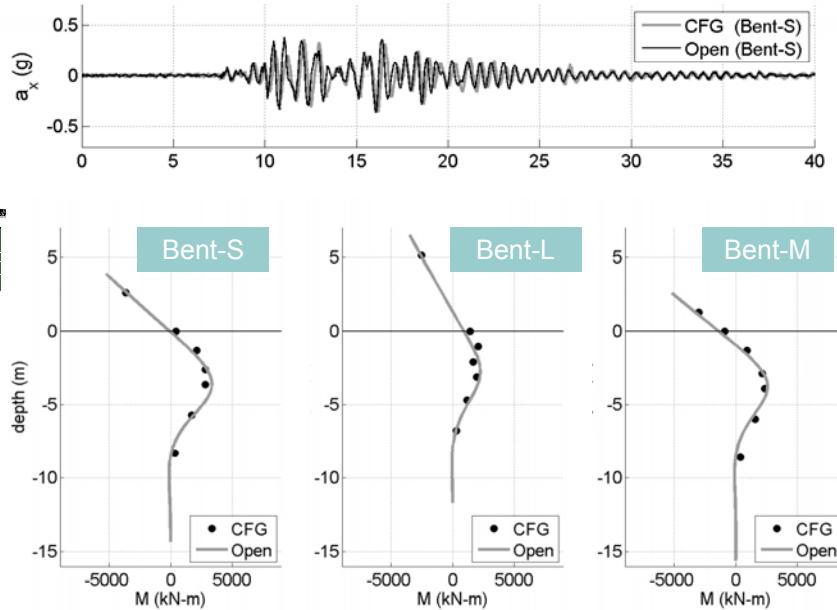
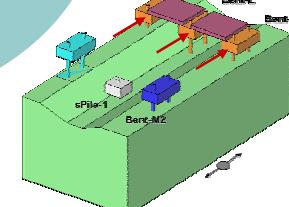
Two-span bridge



Two-span bridge



Two-span bridge



SPSI of a complete bridge system on liquefiable soil



- Five-span bridge
- pile group foundation
- abutment
- liquefiable soil / various layers

Soil-pile-bridge-abutment interaction

- lateral spreading
- earthquake intensities
- uncertainties

Just a couple of runs ☺

Thousands of runs!!! 😞

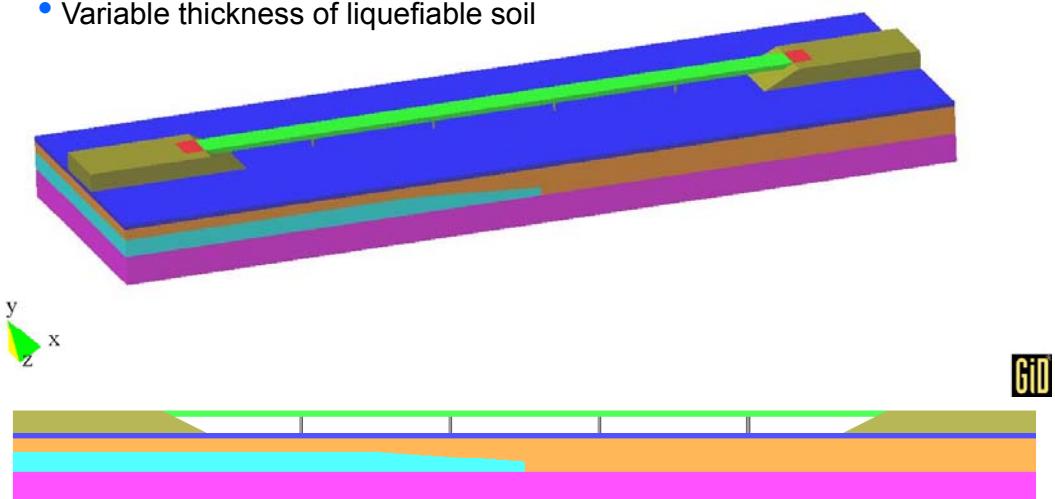
Numerical Simulation of a complete bridge system using OpenSees



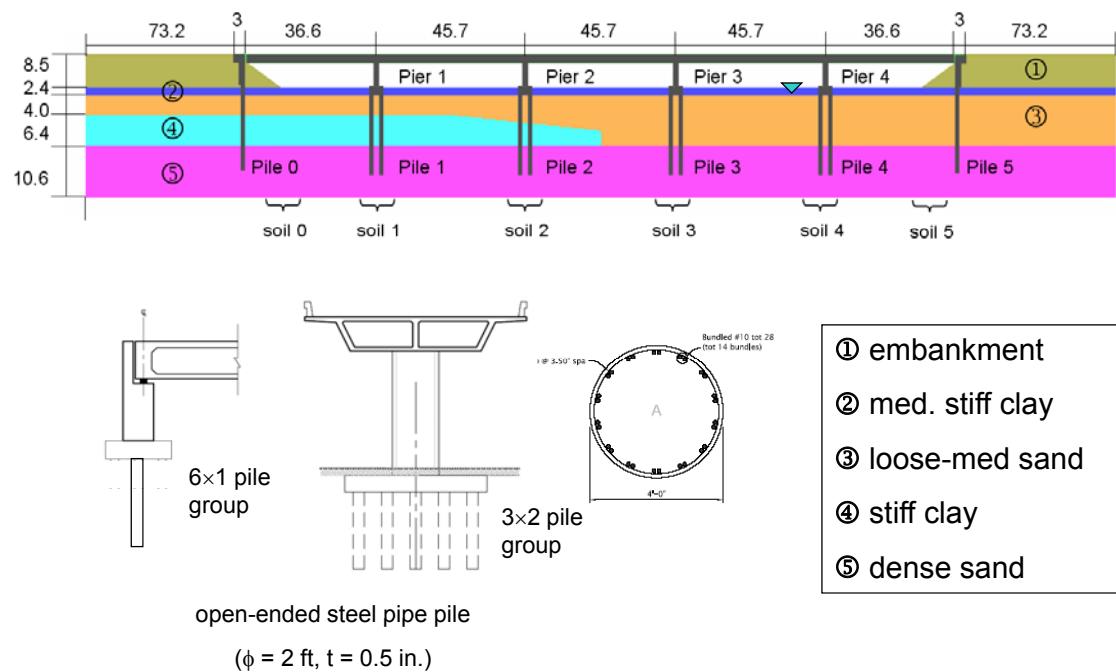
Performance Based Earthquake Engineering

Example: Bridge on liquefiable soil deposit

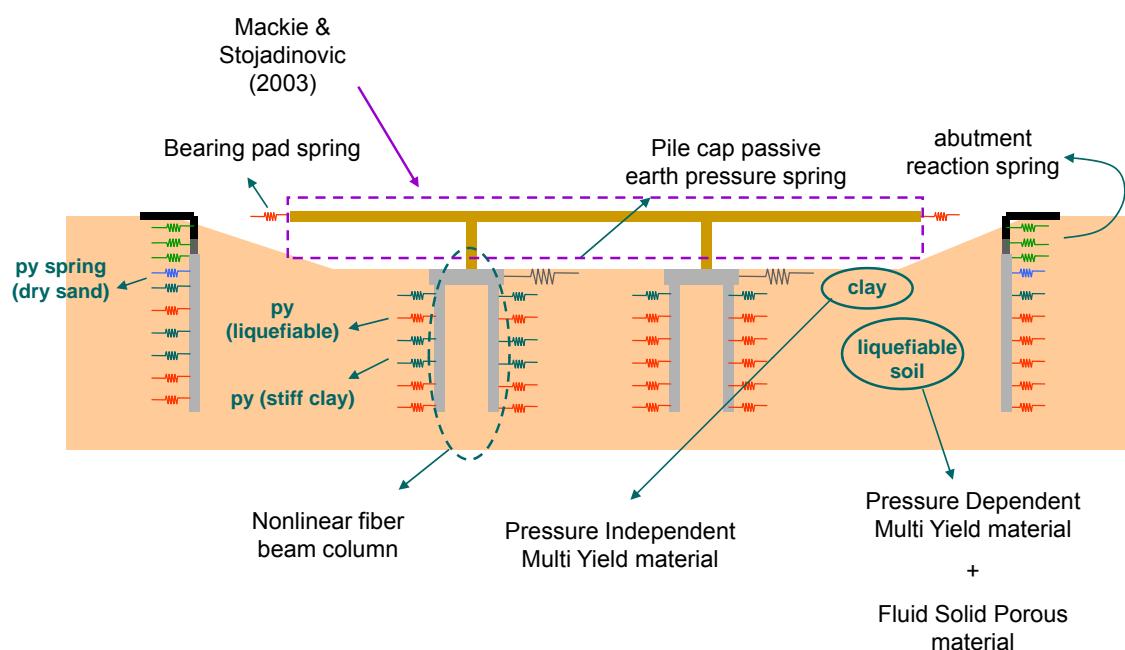
- Five-span bridge
- Approach embankments
- Variable thickness of liquefiable soil



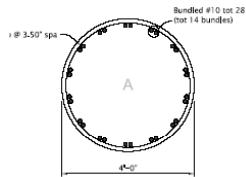
Target bridge system



Numerical modeling for target bridge system

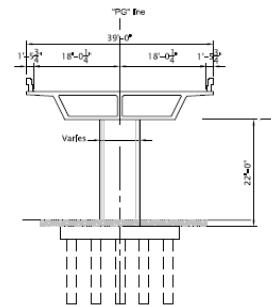


reinforce con'c column
(column A – 4 ft)



prestressed
reinforced con'c
bridge

(type 1 – 22ft)

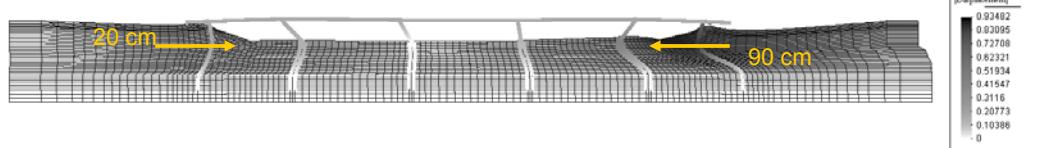


connection

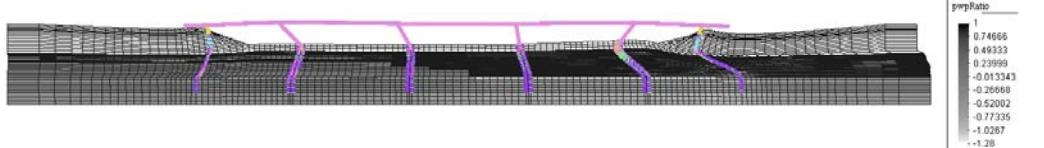


Bridge system response

displacement

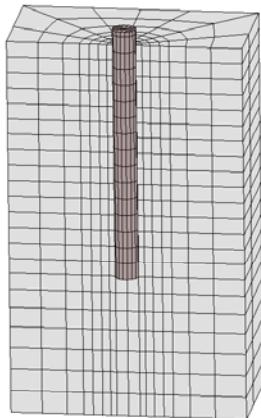


r_u

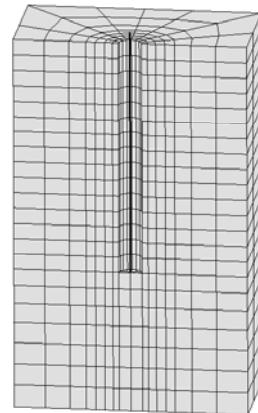


Erzincan, Turkey 1992 ($a_{max} = 0.70g$)

3D Pile Analysis



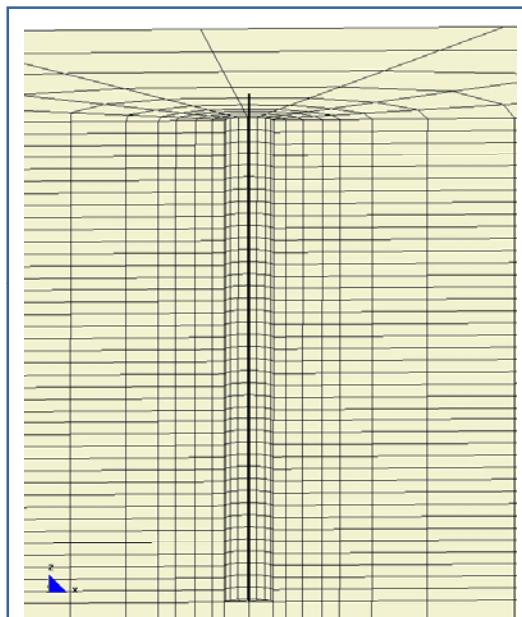
Solid-Solid Model



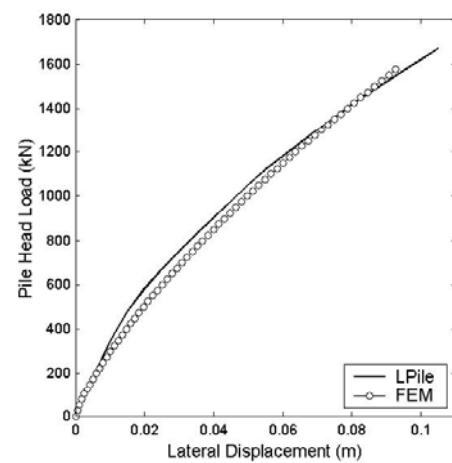
Beam-Solid Model

Laterally Loaded Piles (solid-beam contact element)

- Perform numerical load test



- Compare results



3x Magnification

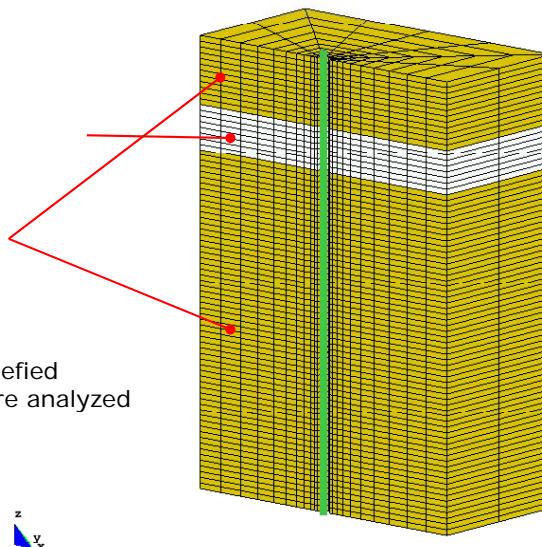
3D Modeling Approach

The soil is modeled with brick elements and a Drucker-Prager constitutive model to capture pressure-dependent strength

Liquefied Layer:
reduced strength

Unliquefied Layers:
dense Sand

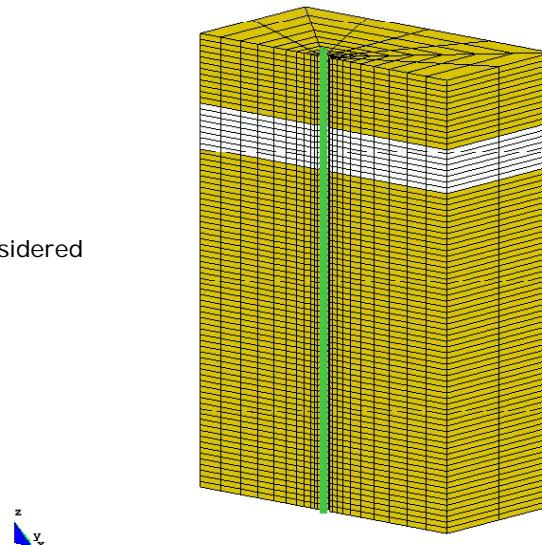
Various combinations of liquefied
layer depth and thickness are analyzed



3D Modeling Approach

The pile is modeled with beam-column elements

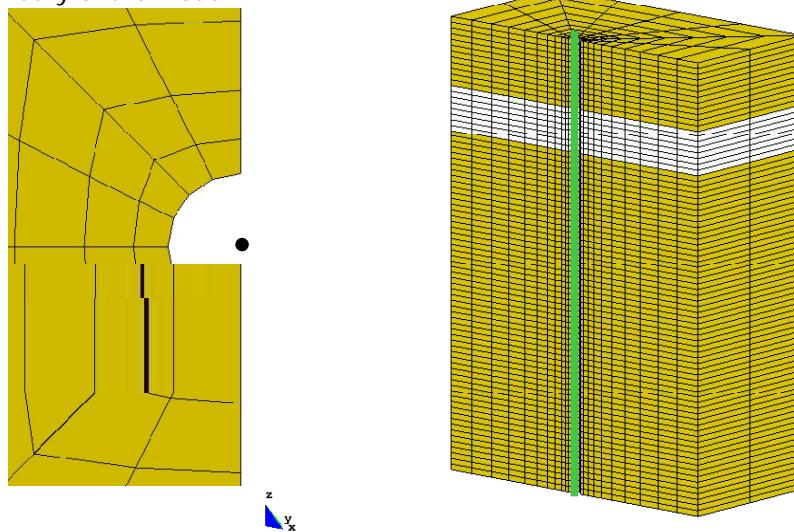
Three **pile diameters** are considered
(0.61, 1.37, 2.5 m)



3D Modeling Approach

Beam-solid contact elements are used to model the soil-pile interface

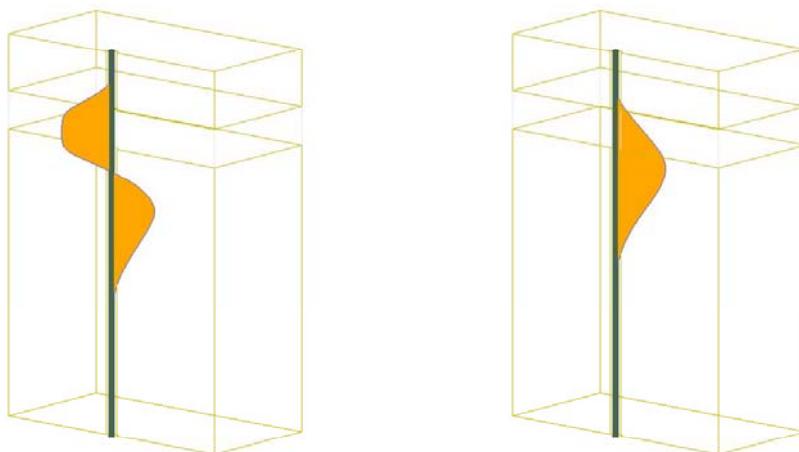
Lateral spreading is modeled by applying a free-field displacement profile to the boundary of the model



Beam-Solid Contact Elements

The beam-solid contact elements enable the use of standard beam-column elements for the pile

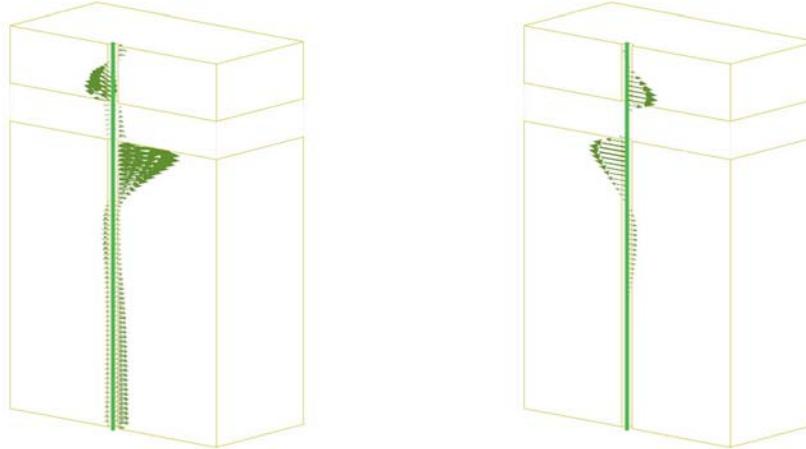
This allows for simple recovery of the shear force and bending moment demands placed upon the pile



Beam-Solid Contact Elements

The beam-solid contact elements enable the use of standard beam-column elements for the pile

Additionally, the surface traction acting on the pile-soil interface can be recovered and resolved into the forces applied by the soil to the pile

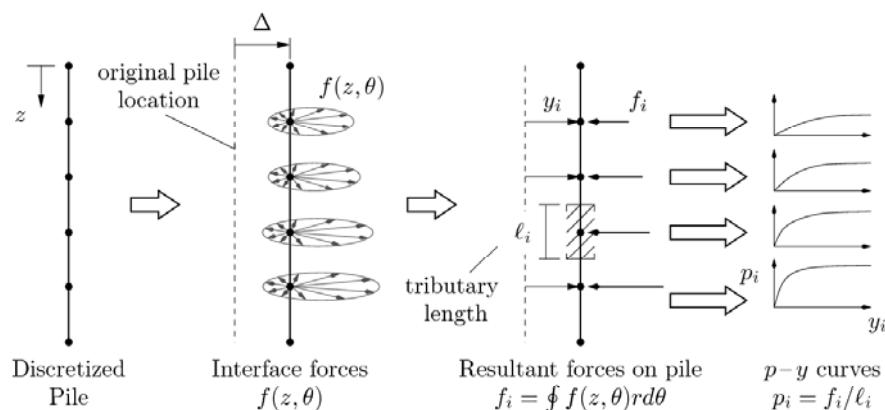


Computing $p-y$ Curves: Rigid Kinematic

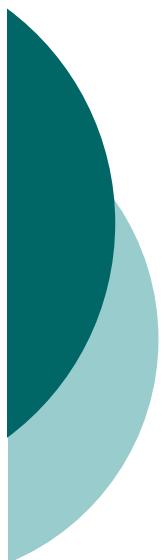
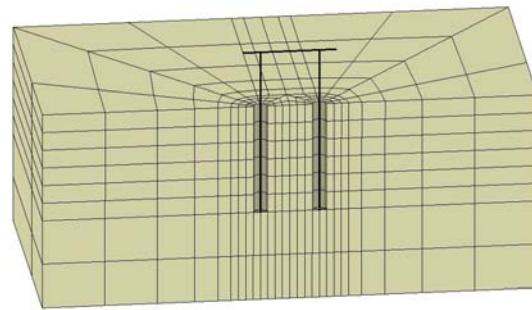
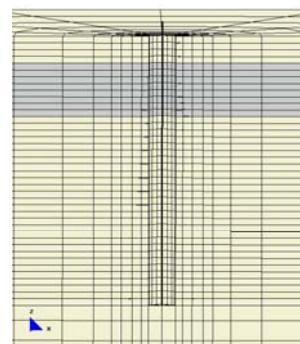
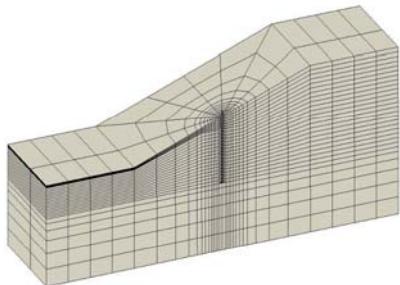
Work with 3D FE models has shown that use of a general pile deformation creates $p-y$ curves which are influenced by the selected pile kinematics

A rigid pile kinematic is used to evenly activate the soil response with depth and to obtain $p-y$ curves which are free from the influence of pile kinematics, reflecting only the response of the soil.

Computational process



Other Applications: Piles in Sloping Ground, Bridge bent analysis



Questions?